

Appendix 2-E - Model Documentation

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91 **Executive Summary**

92 This report presents a preliminary version of the model documentation for the Shasta Watershed
93 Groundwater Model (SWGM) v 1.0; this is the first available integrated hydrological model that
94 represents the entire Shasta Valley watershed. This documentation highlights key model compo-
95 nents and describes the planned modifications considered for future updates of the SWGM. Many
96 of these modifications and enhancements are already under development requiring the technical
97 team to balance the need to document key model inputs or assumptions and the ongoing refine-
98 ment of the SWGM. This effort to document an evolving model has therefore required the technical
99 team to incorporate place holders pending further information. Any updates to parametrization,
100 parameter values, or additional observations will be published in SWGM v1.1. SWGM v1.1 is
101 expected to be released October 2021.

102 As an important note for the review of the GSP, the model has been actively used only to provide
103 a representation of the water budget of the entire watershed and of the groundwater basin for

104 historical, and current conditions and for future climate change scenarios. All key GSP decision
105 up to this point, including the development of Sustainable Management Criteria (SMCs), have
106 been made using available observed data and not on simulated results from the SWGM. The
107 Advisory Committee that collaborated with the technical team throughout the past three years
108 strongly recommended that the GSP clearly state that the development of the SWGM has been
109 an achievement but, due to the limited time and the limited data availability, the uncertainty in the
110 model is currently too significant to be reasonably used to drive critical decision making for the
111 GSP. The extensive data gap section (Appendix 3-A) and the description of the SMCs in Chapter
112 3 explain in detail which data will be collected over the next five years to allow the development of
113 a more robust model. For the 5-year GSP update, we envision new definitions of the SMCs that
114 rely on observed data in addition to simulated model results and future scenarios.

115 A brief history of the development of all the model components is summarized here. The tech-
116 nical team started working on data collection and evaluation in 2018. Following this preliminary
117 assessment, we followed these steps:

- 118 • Development of the 3-dimensional geological model: analysis and geolocation of about 1500
119 well-logs throughout the valley, development of the geological model which serves as the
120 basis for the groundwater model layer definition;
- 121 • Development of the crop-demand soil water budget model (Davids Engineering, Appendix
122 2-1);
- 123 • Extensive coordination with the State Water Resource Control Board (SWRCB) environmental
124 flows project technical team to ensure that atmospheric inputs including precipitation, potential
125 evapotranspiration, and temperature align to the extent possible;
- 126 • Development of a surface water hydrology model reflecting key elements including precip-
127 itation as rain or snow, snow accumulation, snowmelt, and surface runoff using the PRMS
128 software with preliminary sensitivity analysis and calibration;
- 129 • Development of the Hydrogeological Conceptual Model;
- 130 • Groundwater model (based on MODFLOW) with preliminary sensitivity analysis and calibra-
131 tion; and
- 132 • Preliminary coupling in GSFLOW, but not currently used because of runtime limitations.

133 The PRMS surface water model is expected to be refined and enhanced significantly in coming
134 iterations as additional data and datasets become available. Time series datasets derived from an
135 array of planned stream gages is expected to allow for the validation of surface water flows derived
136 from a currently poorly understood combination of precipitation as rain or snow, snow melt, and
137 spring flow. In the absence of a comprehensive and defensible hydrologic feature or hydrography
138 dataset, the modeled representation of stream channels and springs was derived using a digital
139 elevation model (DEM) and Advisory Committee input. This placeholder dataset is expected to
140 be revised and enhanced using a combination of continued stakeholder outreach, validation using
141 satellite imagery, and potentially additional instrumentation. Streambed location and geometry
142 is expected to be revisited and revised with high resolution Light Detection and Ranging (LiDAR)
143 elevation data provided by the SWRCB.

144 The spatial and temporal dynamics of snowpack hydrology within the Shasta Watershed are cur-
145 rently a notable data limitation with significant variability observed at snow pillows across the re-
146 gion and limited understanding of glacier melt on Mt. Shasta. Future DWR snow surveys are
147 expected to allow for refinement of the snow module within PRMS to more effectively simulate
148 the accumulation and subsequent melting of snowpack across the Shasta Watershed. Additional

149 novel resources in the field of snowpack hydrology, including snowpack modeling from UC Santa
150 Barbara's Snow Hydrology Research Group is also expected to allow for the refinement of the
151 snowpack in PRMS.

152 The first iteration of the SWGM includes a series to atmospheric time series datasets that were de-
153 veloped by Paradigm Environmental, the technical team of consultants developing a parallel model
154 for the SWRCB's environmental flows project. An extensive effort was made to coordinate with the
155 SWRCB's technical team through a series of meetings and follow up conversations allowing for
156 the sharing of model inputs but not yet model input documentation. The SWGM technical team
157 has included a short conceptual overview outlining the origin and development of these datasets
158 and how they were incorporated into the PRMS model in the absence of comprehensive docu-
159 mentation from Paradigm Environmental or a SWRCB environmental flows project work product to
160 reference. The refinement of atmospheric inputs is expected to be a key component of SWGM re-
161 visions through a combination of on the ground observed conditions and remote sensing datasets
162 derived from satellites. Key areas of focus are expected to be the spatial and temporal variability
163 of precipitation and temperature as it drives the rain, snow, and snowmelt elements of the model.

164 **Summary of ongoing and future improvements**

165 SWGM v1.0 should be considered a preliminary effort to characterize the Shasta Watershed. Data
166 from continuous groundwater sensors, increased number of stream gages, and agricultural water
167 usage will provide updates to the calibrated values of the system. There are a number of updates
168 that are under consideration for the base model:

- 169 • Updates to glacier melt and snow dynamics on Mount Shasta. Updates to the PRMS code,
170 v 5.2, include a more robust characterization of glacier dynamics. Increased data collection
171 on precipitation, solar radiation, air temperature, and other climate variables should also be
172 included in PRMS updates.
- 173 • Geologic updates to include fracture flow within basalt geology.
- 174 • Hydrogeologic updates to refine anisotropy, storage, and model layer thicknesses.
- 175 • Agricultural demands should be internally calculated within the code. Both Ag package within
176 GSFLOW and FMP package with OWHM are possible codes that can be used.
- 177 • Update to stream morphology using LiDAR data from SWRCB.
- 178 • Representation of the canal network using SFR.
- 179 • Update the model simulation period through 2021 to include new continuous groundwater
180 level data collected as part of the GSP.
- 181 • Surface water diversions can be dynamically linked with priorities to the SFR package to meet
182 surface water demand.

183 **Introduction / Background**

184 The Shasta Watershed Groundwater Model (SWGM) was developed to calculate historical and
185 projected water budgets and to improve understanding of long-term trends in groundwater levels.
186 The SWGM is a loosely coupled groundwater-surface water interaction model. The groundwater
187 is simulated through USGS' Modular Groundwater Flow Model (MODFLOW) (Harbaugh 2005),
188 climate variables and surface water flows are simulated through the Precipitation-Runoff Model-
189 ing System (PRMS) (Markstrom et al. 2008) with the addition of a Daily Root Zone Simulation

190 Model (RSRZ) providing input for irrigated lands (Davids Engineering 2013). The SWGM simu-
191 lates the entire Shasta Valley HUC8 Watershed (Watershed) with the Bulletin 118 Groundwater
192 Basin located within the domain.

193 The SWGM was developed to meet the requirements of the Sustainable Groundwater Manage-
194 ment Act (SGMA) (Cal. Water Code, Division 6, Part 2.74).

195 **Purpose and Scope**

196 Development of SWGM was done to assist in the development of a water balance within the Shasta
197 Valley Groundwater Sustainability District. In order to estimate subsurface inflows into the District,
198 the entire Watershed is modeled. This iteration of the model should still be considered prelimi-
199 nary. Inflows and outflows within the watershed are accounted for to degree that time and budget
200 allowed. Updates to the model should be conducted as additional data are gathered from the
201 region.

202 **Description of Study Area**

203 **Model Software Summary**

204 The SWGM is a combination of multiple models interacting to simulate the entire HUC8 Shasta
205 Watershed. Three models are used to estimate all of the flow components herein. The three
206 models are a Daily Root Zone Simulation Model (RZSM) developed by Davids Engineering, a
207 Precipitation-Runoff Modeling System (PRMS), and MODFLOW-OWHM.

208 *RSRZ*

209 Davids Engineering developed a Daily Root Zone Simulation Model (RSRZ) that calculates the
210 root zone water budget based on the water budget components Figure 1. The RSRZ uses pre-
211 cipitation and evapotranspiration as the driving water budget model inputs, and root zone water
212 balance parameters based on crop and soil type that impact the soil moisture storage. The RSRZ
213 model relies on remote sensing-based estimates of evapotranspiration model derived from imagery
214 collected by LandSat satellties, Parameter-elevation Regressions on Independent Slopes Model
215 (PRISM) rainfall data developed by Oregon State University¹, and root zone parameters based
216 on the crop and soil types (Davids Engineering 2013). The Daily root zone dynamics were mod-
217 eled from January 1989 to December 2018. Daily water budget components were then upscaled
218 to monthly values by taking the sum of each water budget component (e.g. evapotranspiration).
219 These monthly values were extracted and incorporated into the MODFLOW models as *Applied*
220 *Water* and *Deep Percolation* which respectively represent the amount of groundwater pumping for
221 cells where irrigation occurs and the amount of groundwater recharge to the aquifer. Complete
222 details of the Daily Root Zone Simulation Model can be found in Chapter 2 Appendix E.

223 Davids Engineering developed a Daily Root Zone Simulation model that uses remote sensing
224 based evapotranspiration model using LandSat, PRISM rainfall data from Oregon State², and root
225 zone parameters based on the crop and soil types (Davids Engineering 2013). The Daily RSRZ
226 was ran from January 1989 to December 2018 and provided the calculated *Applied Water* and

¹PRISM website: <http://prism.oregonstate.edu/>

²PRISM website: <http://prism.oregonstate.edu/>

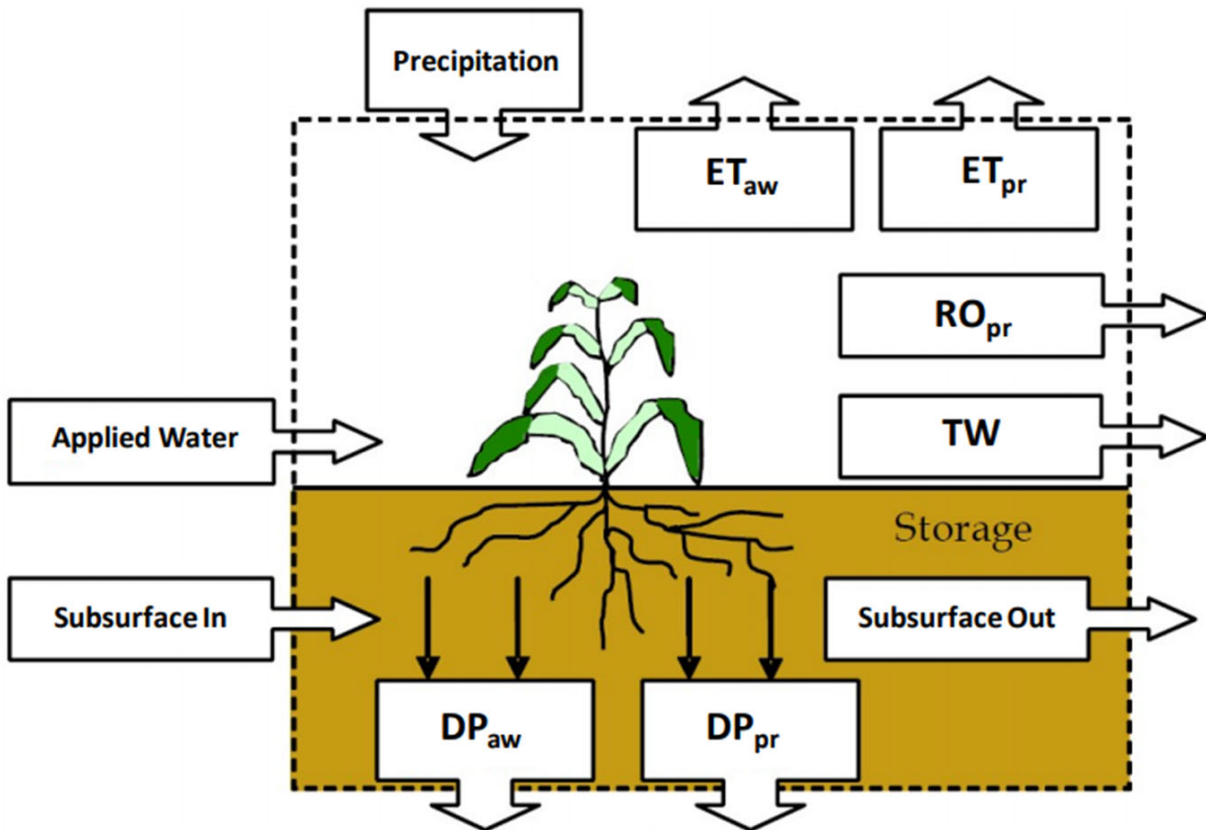


Figure 1: Conceptualization of Fluxes of Water Into and Out of the Crop Root Zone

227 *Deep Percolation* which respectively represent the amount of groundwater pumping for irrigated
 228 cells and the amount of groundwater recharge to the aquifer. The daily water budget compo-
 229 nents were then upscaled to monthly values by taking the sum of each water budget component
 230 (e.g. Evapotranspiration). Complete details of the Daily Root Zone Simulation Model can be found
 231 in Chapter 2 Appendix E.

232 *PRMS*

233 PRMS is a surface water hydrology model focused on simulating a watershed's response to climatic
 234 processes such as precipitation, evaporation, and evapotranspiration. The first iteration of PRMS
 235 was released by USGS in 1983 in the FORTRAN programming language where model inputs were
 236 incorporated with punch cards and outputs were summarized by line printers. USGS has released
 237 five iterations of the model with recent revisions focused on streamlining the integrating PRMS with
 238 other computational tools such as USGS' MODFLOW. The surface water component of USGS'
 239 coupled Groundwater and Surface Water FLOW (GSFLOW) model developed for the Shasta GSP
 240 is the most recent publicly available iteration of PRMS, PRMS-V or version 5, released in late
 241 May of 2019. PRMS is comprehensively documented and supported by USGS with a dedicated
 242 webpage, release notes, and installation instructions. The PRMS version 4 User's Manual (PRMS
 243 User's Manual) is the most comprehensive resource outlining model parameters and processes.
 244 Table 1 documents the process and modules used within the SWGM.

245 *MODFLOW*

Table 1: PRMS Modules used

| Process | Module |
|------------------------------|----------------------|
| Computation Order | <i>call_modules</i> |
| Basin Definition | <i>basin</i> |
| Cascading Flow | <i>cascade</i> |
| Common States and Fluxes | <i>climateflow</i> |
| Potential Solar Radiation | <i>soltab</i> |
| Parameter Setup | <i>setup_param</i> |
| Timestep Control | <i>prms_time</i> |
| Time Series Data | <i>obs</i> |
| Potential Evapotranspiration | <i>climate_hru</i> |
| Temperature Distribution | <i>temp_1sta</i> |
| Precipitation Distribution | <i>precip_1sta</i> |
| Solar Radiation Distribution | <i>ddsolrad</i> |
| Transpiration Distribution | <i>transp_tindex</i> |
| Canopy Interception | <i>intcp</i> |
| Snow Dynamics | <i>snowcomp</i> |
| Surface Runoff | <i>srunoff_smidx</i> |
| Soilzone Computations | <i>soilzone</i> |
| Groundwater | <i>gwflow</i> |
| Streamflow Routing Init | <i>routing</i> |
| Streamflow Routing | <i>muskingum</i> |

246 MODFLOW is a finite difference groundwater model simulating spatial and temporal groundwater
247 conditions in the watershed. The MODFLOW model simulates the spatially and temporal variable
248 dynamics of groundwater fluxes and groundwater elevations which are sufficient to characterize a
249 water budget for the Basin and determine whether there will be significant changes in water level
250 that may impact groundwater users. Table 2 summarizes the MODFLOW packages used within
251 SWGM.

Table 2: MODFLOW Packages used to Calculate Groundwater Flows in the Basin

| MODFLOW Package | Application |
|------------------------|--|
| BAS6 | Define Active Model Domain |
| DIS | Define Model Grid and Extent |
| LAK | Lake Shastina and Grass Lake |
| SFR | Shasta River, tributaries, and springs |
| UPW | Geologic model |
| GHB | Canals |
| UZF | Recharge and runoff |
| WEL | Groundwater pumping for irrigation needs |
| ZONE | Delineate hydrogeologic zones |
| PVAL | Parameters data |
| GAGE | Output from SFR and LAK packages |
| OC | Output control |
| NWT | Numerical solver |
| HOB | Head observation package |

252 Hydrologic System

253 Climate

254 The Shasta Valley generally has a mixture of warm-summer Mediterranean and high desert envi-
255 ronment climates with distinctive seasons of cooler, wetter winters and warm, dry summers. The
256 orographic effect of the mountains to the west and south sides of the Valley creates a rain shadow
257 in eastern areas of the Valley. The higher elevation areas to the west and south of the Valley
258 historically receive greater annual precipitation (30–70 inches [in], or about 76–177 centimeters
259 [cm]) in comparison to annual precipitation on the east side of the Valley (12–15 in). Annual mean
260 precipitation ranges from a low of about 13 to 15 in (33–38 cm) at lower elevations to a high of
261 about 67 in (170 cm) at Mount Shasta; see the summary statistics table for the (out of Watershed
262 but close to the southern border) Mount Shasta rainfall gauge (station ID: 045983; SWRCB 2018).
263 In the City of Yreka, annual precipitation averages range from 19 to 21 in (48–53 cm); see the
264 attached plot of 1960–2005 Yreka annual precipitation (CDWR 2011) and the summary statistics
265 table for the Yreka rainfall gauge (station ID: 049866; SWRCB 2018). Annual precipitation ranges
266 from 25 to 29 in (64–74 cm) at 853 higher elevations of the Klamath Mountains to the west, and up
267 to 33 in (84 cm) near China Mountain. To the east, higher elevations of the Cascade Range receive
268 from 19 to 27 in (48–69 cm) of precipitation annually. The rainy season, which generally begins in
269 October and lasts through April, accounts for about 80 percent of total annual rainfall. At elevations
270 below 4,000 ft (~1,200 m) amsl, precipitation mostly occurs as rainfall, as is the case on the valley
271 floor. Precipitation accumulates as snow in the surrounding mountains, with a rain-snow transition
272 zone from 4,000 to 5,000 ft (~1,200–1,500 m) amsl. Accumulation of snowfall in the surrounding
273 mountains results in runoff during spring snowmelt.

274 **Surface Water**

275 Elevation across the approximately 800 sq mi (~2,070 sq km) Watershed ranges from just over
276 2,000 ft (610 m) amsl near the confluence with the Klamath River to over 14,000 ft (4,300 m)
277 near the peak of Mount Shasta. Several smaller watersheds encompassed by the Shasta River
278 watershed; the two most notable being the Little Shasta River and Parks Creek. The Watershed is
279 bounded to the west by the Scott River watershed, to the south by the Sacramento River watershed,
280 to the east by the Butte Creek watershed, and by the Klamath River to the north. Shasta River
281 is approximately 58 miles (93 km) long stretching from the peak of Mount Eddy at about 9,000
282 ft (2,750 m) amsl to the confluence with the Klamath River. The Little Shasta River drainage
283 basin within the Watershed is bounded by Goosenest Mountain (8,260 ft; 2520 m amsl) to the
284 south, Ball Mountain (7,792 ft; 2,375m amsl) to the east and Willow Creek Mountain (7,828 ft;
285 2386 m amsl) to the north. Little Shasta River is predominantly spring fed, sustained by a series of
286 springs emerging from Quaternary and Tertiary High Cascade volcanic materials, discussed further
287 in Section 2.2.1.3. Mount Shasta, snow-covered year-round, is the most conspicuous feature of
288 the landscape, visible from all parts of the Valley. Several glaciers stretch along its upper slopes
289 which are the primary source of recharge to the Basin. On its north slope, Whitney, Bolam, and
290 Hotlum Glaciers descend to altitudes of about 10,000 ft (3,048 m) amsl. On the south slope, the
291 Koiwakiton Glacier descends to an altitude of 12,000 ft (3,658 m) amsl, and the Clear Creek and
292 Winton Glaciers to about 11,000 ft (3,353 m) amsl. Regional climate models generally predict the
293 loss of Mount Shasta's glacier volume over the next 50 years and total loss of the glacier by the
294 year 2100, likely resulting in reduced recharge in the Basin (UCD 2010?).

295 The Shasta River has a complicated seasonal and longitudinal flow regime due to intricate surface
296 water and groundwater interactions, coupled with extensive agricultural diversion and return flows
297 (Vignola and Deas 2005; Nichols et al. 2010). The Watershed includes a small number of small-
298 scale diversion dams and diversions of the Shasta River or major tributaries, with the two main
299 sources of water being the Shasta River and Parks Creek with storage in Lake Shastina (Dwinnell
300 Reservoir). A number of the small-scale diversion dams have been or are in the process of being
301 removed or modified for fish passage. Water rights dictating usage throughout the Shasta Basin are
302 a combination of riparian and appropriative water rights adjudicated as a part of the 1932 Decree
303 (CDWR 1932). Buck (2013) constructed a groundwater model for a portion of the Watershed and
304 summarized major balance components for the period 2008–2011. The upper Shasta River (i.e.,
305 upstream of Dwinnell Dam) originates on the eastern slope of Mt. Eddy and is characterized by a
306 runoff-driven hydrograph derived from rainfall and snowmelt (Nichols et al. 2010). Inflows to Lake
307 Shastina consist of the upper Shasta River, flows diverted from Parks Creek near Edgewood, and
308 Carrick Creek originating from the northwest flank of Mount Shasta. In 1928, construction of Dwin-
309 nell Dam was completed, impounding Lake Shastina to primarily serve as a storage reservoir and
310 diversion for agricultural irrigation water throughout the Valley. Lake Shastina is the largest single
311 water source in the Watershed. Outflow from Lake Shastina to the lower Shasta River, regulated
312 by Dwinnell Dam, has reduced mean annual discharge in the reaches immediately downstream of
313 the reservoir by up to 90 percent (Jeffres et al. 2008; Nichols 2008; Nichols et al. 2010). Maximum
314 reservoir storage capacity in Lake Shastina is rarely achieved because of the permeable underly-
315 ing volcanoclastic rocks which allow impounded water to flow into the underlying aquifer (Vignola
316 and Deas 2005). Mack (1960) reported that multiple springs along the base of the ridge forming
317 the western embankment of Lake Shastina increased in flow following construction of the reservoir.
318 Seepage losses from Lake Shastina have been estimated at 6,500 to 42,000 acre-feet (AF) (~8-
319 52 million cubic meters (m³)) annually, significant relative to the reservoir's 50,000 AF (~62 million

m³) storage capacity, representing a loss of 13 to 84 percent of storage capacity (Paulsen 1963, NCRWQCB 2006). Flows in the lower Shasta River (i.e., downstream of Dwinnell Dam) are composed of minimal releases from Lake Shastina, tributary creeks (e.g., Parks Creek, Willow Creek, Little Shasta River), multiple discrete groundwater springs (e.g., Big Springs, Little Springs, Clear Springs, Kettle Springs, Bridge Field Springs), and additional diffuse groundwater springs. The lower Shasta River is characterized by a spring-dominated hydrograph primarily sourced from Big Springs Creek, supplied by multiple groundwater springs in the Big Springs Complex vicinity (Jeffres et al. 2008, Nichols 2008, Nichols et al. 2010). Spring-fed baseflows from Big Springs Creek outside the irrigation season (i.e., November to March) are five times those of the lower Shasta River upstream of the Big Springs Creek confluence (including Parks Creek) for the same time period (Jeffres et al. 2009). Approximately 95 percent of baseflows during irrigation season (i.e., April to October) in the lower Shasta River originate from the Big Springs Complex. During irrigation season, Big Springs Creek baseflows are approximately 35 percent lower, caused by temporally variable irrigation diversions and unquantified groundwater pumping (Jeffres et al. 2009). Instream flows downstream of Big Springs Creek confluence quickly rebound to spring-fed baseflow conditions following irrigation season (Nichols et al. 2010). Dwinnell Dam (constructed in 1928) is the largest water storage structure in the Basin, with current¹ capacity of 50,000 AF (~62 million m³), upgraded from 36,000 AF (~44 million m³) in 1965 (USFWS15422013). Water is delivered to users in Shasta Basin via canals, diversion facilities, pumps, and storage infrastructure (Willis et al. 2013). The largest storage and delivery systems in the Shasta Basin are maintained by water service agencies or private water users which operate in accordance with the Watermaster service requirements (Willis et al. 2013). Major diversions and smaller dams or weirs are located below Dwinnell Dam, along with numerous diversions on tributaries (CDFW15471997; Lestelle 2012; NOAA Fisheries 2014; CDFW 2016). Several diversions and return channels exist largely for agricultural purposes that primarily operate during the irrigation season (April 1-September 30), including the Grenada Irrigation District Ditch, the Shasta River Water Association, and Oregon Slough (Jeffres et al. 2010) (Figure 32). The City of Yreka obtains much of its water supply from Fall Creek (Figure 33), located outside the Watershed near Iron Gate Reservoir (Pace Engineering 2016). The City's treated wastewater, totaling 966 AF (1.2 million m³) in 2015, is discharged to percolation fields near Yreka Creek (Pace Engineering 2016). Historical instream flow data were collected from the United States Geological Survey (USGS) and California Department of Water Resources (DWR) Water Data Library and California Data Exchange Center (CDEC). Two (2) USGS streamflow gauges (stations SRM and SRY) are present in the Watershed with observed data spanning water years 1958 to 1978, and 2002 to 2016. Five additional gauging stations are maintained by DWR and are associated with sporadic data collection in two to three-year periods. Gauge locations in the Watershed are shown in Figure (Figure33). Data were analyzed to assess quantity and quality of the observed record. Quantity was measured as percent of days with recorded flow data at each gauge, and quality was assessed as percent of days flagged by USGS as having been "edited or estimated by USGS personnel (USGS 2018)."Table (?; Table: Summary of streamflow data quantity and quality in the Shasta Valley Groundwater Basin) provides a summary of USGS data quantity and quality in the Watershed; a continuous flow record of reliable data (in terms of quantity and quality) is present throughout the watershed from 1957 to present. In 2005 and 2009, the Nature Conservancy acquired property in the Watershed, and at this time the University of California at Davis Center for Watershed Science, the Nature Conservancy, and Watercourse Engineering began monitoring streamflow in Big Springs Creek, the mainstem Shasta River, and Little Shasta River (Jeffres et al. 2008, 2009, 2010; Nichols et al. 2016, 2017; Null et al. 2010; Willis et al. 2012, 2013, 2017). Additional sources of flow data include gauges placed on the Shasta River and Parks Creek in 2001 and 2002 (Watercourse Engineering 2006); estimates

368 of unimpaired flows (Deas et al. 2004); a 2016 water balance study (SVRCD 2016); summaries of
369 discrete flow measurements for springs in the Watershed including Little Springs Creek (Deas et
370 al. 2015) and Big Springs Creek (Appendix G of NCRWQCB15752006); measurements of springs,
371 creeks, and diversions on the Shasta Springs Ranch (Chesney et al. 2009, Davids Engineering
372 2011); and a compilation of data for sites in the Little Shasta River drainage basin (CDFW 2016).
373 Streamflow data from all available sources will be further assessed during hydrologic model de-
374 velopment to identify important critical conditions. Data quantity and quality impact both selection
375 of data to be used for calibration and interpretation of model performance during associated time
376 periods. More weight will be given to locations and time periods with higher quantity and quality
377 of data. Instream flows in the Watershed have been significantly affected by water resource man-
378 agement in the Basin. Seasonal low flow and drought conditions naturally occur in the watershed,
379 but are becoming more common. Studies have been conducted to characterize hydrology and
380 hydrologic habitat in the Watershed and to determine interim and minimum instream flow needs
381 in the Watershed (McBain & Trush 2013, CDFW 2017). The Instream Flow Needs study docu-
382 mented historical and current sampling above and below Parks Creek confluence, in the center of
383 the Watershed 1588 (McBain & Trush 2013). Historical data of unimpaired mean monthly flow in
384 the Upper Shasta River and Parks Creek estimate a maximum of approximately 208 cubic feet per
385 second (cfs) (~6 cubic meters per second (m^3/s)) and a minimum of 6 cfs (~0.2 m^3/s) during spring
386 and summer months. Baseflows in spring and summer 2010 recorded a maximum of 36 cfs (~1
387 m^3/s) and a minimum of 5.6 cfs (0.16 m^3/s ; see Figure: Historic stream flows at notable gauges
388 along the Shasta River and Parks Creek). According to these studies, considerable inter-annual
389 streamflow variability exists along with uniformity and predictability of streamflow between June
390 and late October, consistent with other streams in the region.

391 **Groundwater**

392 The groundwater system is poorly understood in the Shasta Watershed. The complex geology is
393 further discussed in Appendix 2-A In general groundwater flow is consistently towards the Shasta
394 River in the middle of the watershed with an overall trend of flow to the north towards the Klamath
395 River. The groundwater flow is further complicated by fracture flow within fractured basalt in the
396 southeast area of the watershed. Groundwater is known to be connected in the majority of the
397 Shasta River with groundwater daylighting at multiple springs near the Big Springs Complex.

398 **Model Development**

399 **Climate Data**

400 The following section provides an overview of the atmospheric time series inputs that drive the
401 simulation of the energy and water balance of hydrologic response units (HRUs) within the PRMS
402 model.

403 **Climate Inputs**

404 **Precipitation** Precipitation time series were manually processed by Paradigm Environmental us-
405 ing geographic information system (GIS) and software packages before being assigned to each

406 HRU within the Shasta PRMS model domain. Hourly modeled precipitation totals were extracted
407 for the 29-year modeled period of record from the National Aeronautics and Space Administration
408 (NASA) North American Land Data Assimilation System (NLDAS)³. NASA developed the NDLAS
409 system to use the best available climatic land surface observations to construct a quality-controlled
410 land surface model (LSM) for the U.S. NLDAS models conditions at a scale of 1.0 degree (approx-
411 imately 84 kilometers longitude and 111 kilometers latitude) for data from 1979 to present and 0.25
412 degree (approximately 21 kilometers longitude and 27.75 miles latitude) from 2000 present.

413 Paradigm Environmental scaled hourly precipitation datasets for each NLDAS grid cell to align
414 with monthly rainfall totals derived from the PRISM model⁴, a high-resolution climate model devel-
415 oped and maintained by Oregon State University. PRISM applies a weighted regression scheme to
416 model climatic conditions with a focus placed on complex regimes where factors such as orography
417 (elevation driven), rain shadows, temperature inversions, slope aspect, and coastal proximity yield
418 unique climates. The PRISM dataset is presented in “climatologies” at a scale of 30-arcsec (800
419 meters) and monthly data are available at 2.5 arcmin (4 km) resolution. NLDAS hourly data were
420 used as relative hyetographs to distribute monthly PRISM totals. Hourly PRISM-scaled NLDAS
421 totals were summed by day and manually assigned to PRMS HRUs corresponding to the centroid
422 of each PRISM grid. The precip_1sta module was used to interpolate and distribute daily precip-
423 itation totals to HRUs between PRISM centroid grids using monthly correction factors to account
424 for differences in altitude, spatial variation, topography, and measurement gage efficiency.

425 **Temperature** Hourly modeled temperature time series were extracted from NLDAS records and
426 post-processed by Paradigm Environmental to represent maximum and minimum temperatures
427 by day. These daily maximum and minimum temperature timeseries were manually assigned to
428 PRMS HRUs corresponding to the centroid of each NLDAS grid. Daily maximum and minimum
429 temperatures were adjusted based on temperature zones. The temp_1sta module was used to
430 interpolate and distribute daily maximum and minimum temperatures to HRUs between NLDAS
431 grid centroids using an estimated monthly lapse rate.

432 **Potential Evapotranspiration** Potential evaporation time series were manually processed by
433 Paradigm Environmental using GIS and software packages. Hourly modeled evapotranspiration
434 time series were extracted from NLDAS records, and manually assigned to PRMS HRUs corre-
435 sponding to the centroid of each NLDAS grid. The climate_hru module was used to read daily
436 evapotranspiration depths directly into PRMS by HRU.

437 **Internal Climate**

438 **Solar Radiation** Daily solar radiation was internally calculated based on the ddsolrad module
439 within PRMS. The ddsolrad module distributes solar radiation to each HRU using a maximum
440 temperature per degree-day relationship discussed extensively in the Solar-Radiation Distribution
441 Modules section of the PRMS model documentation. Maximum assumed temperature within the
442 PRMS model is used to establish a degree-day coefficient based on a relationship established by

³Additional information regarding the North American Land Data Assimilation System (NLDAS) can be found at:
<https://ldas.gsfc.nasa.gov/nldas>

⁴Additional information regarding PRISM model can be found at: <https://prism.oregonstate.edu/>

443 Leavesley and others in 1983. This degree-day coefficient is then used to translate potential short-
444 wave solar radiation to assumed short wave solar radiation with the driving assumption being that
445 higher temperatures correspond to summer months and longer days with higher solar radiation.
446 Conversely, lower maximum temperatures correspond to winter periods with shorter days and
447 lower short-wave solar radiation.

448 **Snow** Precipitation falling within the Shasta Watershed is partitioned in rain, snow, or a mix of rain
449 and snow based on internal parameters established within PRMS. Precipitation occurring on a day
450 where both the minimum and maximum daily temperature are above a threshold where all precip-
451 itation falling is assumed to be rainfall, parameter `tmax_allrain`, is simulated as only rainfall. Sim-
452 ilarly, precipitation falling on days where both the minimum and maximum daily temperatures are
453 below a threshold where all precipitation falling is assumed to be snow, parameter `tmax_allsnow`,
454 is simulated as only snowfall.

455 When the assumed maximum daily air temperature falls between the `tmax_allsnow` and
456 `tmax_allrain` thresholds and the minimum daily air temperature is less than or equal to the
457 `tmax_allsnow` threshold, precipitation is modeled as a mixture of rain and snow. A compre-
458 hensive discussion of the simulation of precipitation as rain and snow can be found in the
459 Precipitation-Distribution Modules section of the PRMS Users Manual.

460 The PRMS model simulates snowpack hydrology processes within the Snow module (`snowcomp`)
461 including snow initiation, accumulation, and depletion by HRU. The Snow module simulates
462 snowmelt as a function of the daily water and energy balance for each HRU including the accumu-
463 lation, sublimation, and melt of snowpack. PRMS computes daily snowpack dynamics including
464 snowpack depth, density, snow water equivalent (SWE), snowpack, temperature, albedo, and
465 cover area to allow users to readily compare modeled representations to key on-site snowpack
466 observations from snow pillows or snow courses as well as satellite-derived observations for
467 factors such as snowpack albedo.

468 Watershed Parameters

469 PRMS requires users to translate the physical characteristics of a subject watershed and rele-
470 vant dynamic temporal elements (e.g., precipitation) into a representation that can be simulated
471 using the quantitative relationships within the modeling platform. The process of translating phys-
472 ical characteristics such as elevation, land use or land cover, geology, and subwatersheds into a
473 set of unique hydrologic units is often referred to as spatial discretization. The process of trans-
474 lating atmospheric conditions into time series that can drive a model is typically referred to as
475 temporal discretization. Both of these processes are discussed below with each section providing
476 an overview and referring readers to more comprehensive discussions in model documentation
477 where available.

478 A key element of PRMS model development is the parameterization of a network of HRUs, stream
479 segments or reaches, and lakes reflecting the understanding of the watershed model domain.
480 HRUs are developed as a function of land use or land cover, soil, elevation, slope, aspect, and
481 climate patterns and are assumed to be uniform in how they respond to atmospheric time se-
482 ries inputs. While PRMS is capable of integrating irregular or complex (non-rectangle) geometry
483 HRUs, USGS strongly recommends that HRUs reflecting the discretization of the land surface align

484 with the subsurface discretization represented in the coupled MODFLOW groundwater model dis-
485 cussed in Section 3.2.1.

486 The Shasta PRMS model is comprised of 42,586 18-acre HRUs arranged in 214 rows and 199
487 columns of a grid. Each HRU is assigned a unique set of land use/landcover and atmospheric
488 inputs during spatial processing using an external GIS. The distribution of HRUs representing the
489 discretized model domain for the Shasta PRMS model is presented in Figure 4.

490 **Elevation and Runoff**

491 A 10-meter resolution digital elevation model (DEM) was extracted from the USGS National Ele-
492 vation Dataset (NED) to represent topography within the Shasta Watershed. This gridded repre-
493 sentation of elevation was translated into mean elevation, slope, and aspect for each HRU and
494 incorporated into the PRMS model.

495 **Soils**

496 The spatial distribution of soils within the Shasta Watershed were extracted from the Natural
497 Resources Conservation Service (NRCS) Soil Survey Geographic (SSURGO) database (addi-
498 tional information regarding the SSURGO database can be found at [https://www.nrcs.usda.gov/
499 wps/portal/nrcs/detail/soils/survey/?cid=nrcs142p2_053627](https://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/survey/?cid=nrcs142p2_053627)). SSURGO presents soil characteris-
500 tic and soil hydraulic summaries including percent sand, silt, clay, as well as available water holding
501 capacity. Relevant hydraulic parameters were used to parameterize the soil-zone module and the
502 soilzone process within PRMS. A comprehensive discussion of the simulation of precipitation as
503 rain and snow can be found in the Soil Zone Module section of the PRMS Users Manual.

504 **Vegetation**

505 There are 5 types of vegetation cover within PRMS, bare soil, grasses, shrubs, trees, and conif-
506 erous correlating to 0 through 4, respectively. The vegetation types are generalized and interact
507 with other variables to account for native vegetation water consumption and use. Distribution of
508 vegetation type is shown on Figure 2.

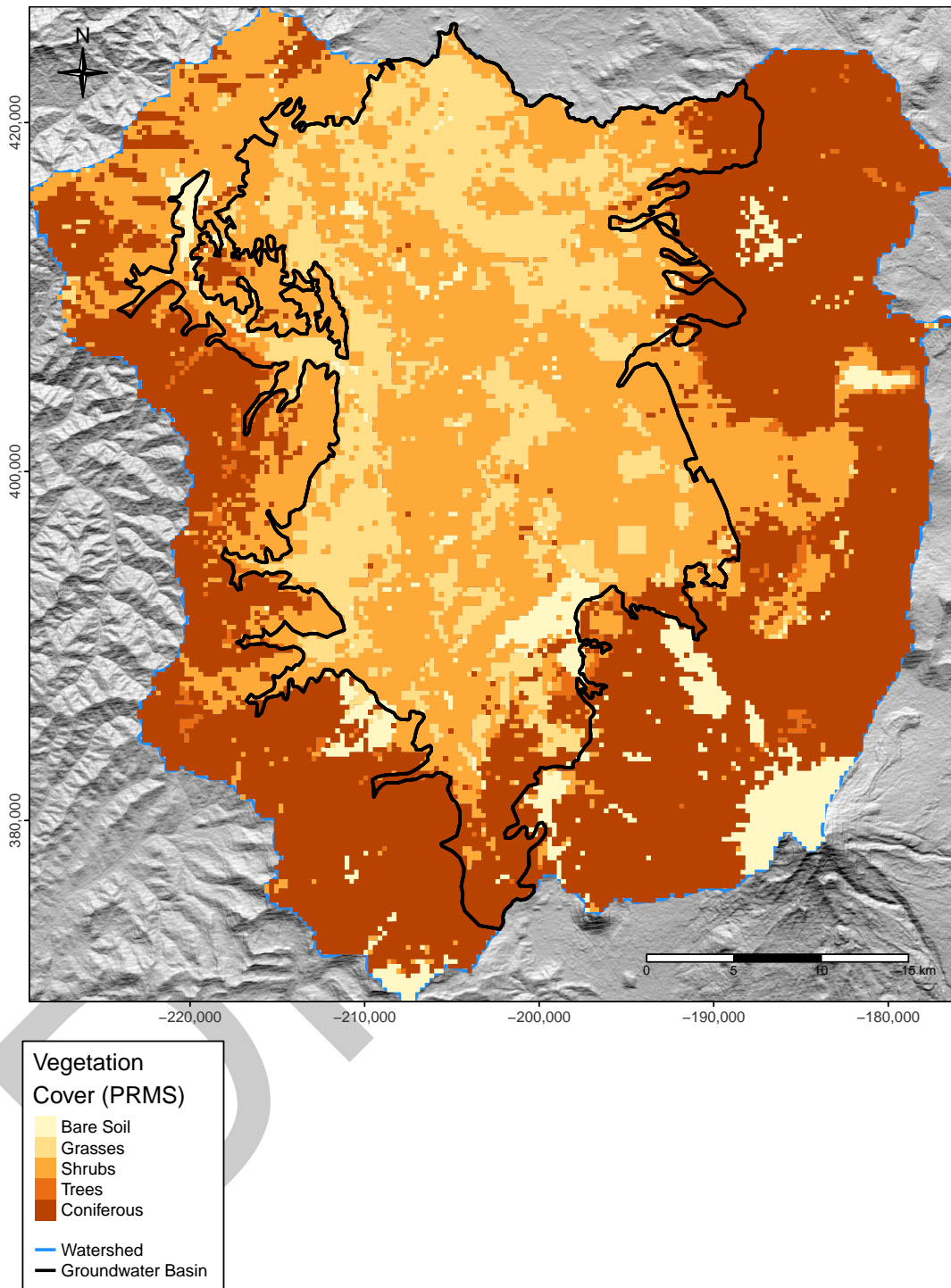


Figure 2: Vegetation type as simulated within PRMS.

509 Discretization

510 Spatial Discretization and Layering

511 The MODFLOW and PRMS models use the same grid consisting of 18 acre (270 meter x 270
 512 meter) grid cells. The active portion of both surface water and groundwater is the HUC8 watershed
 513 boundary. Vertical discretization was carried out to keep layer thicknesses consistent throughout
 514 the model domain due to the amount of discontinuous volcanic geology. Layer 1 top is defined at
 515 land surface and extends 10 meters below land surface. Layers 2 through 4 are 40 meters, 100
 516 meters, and 350 meters thick, respectively.

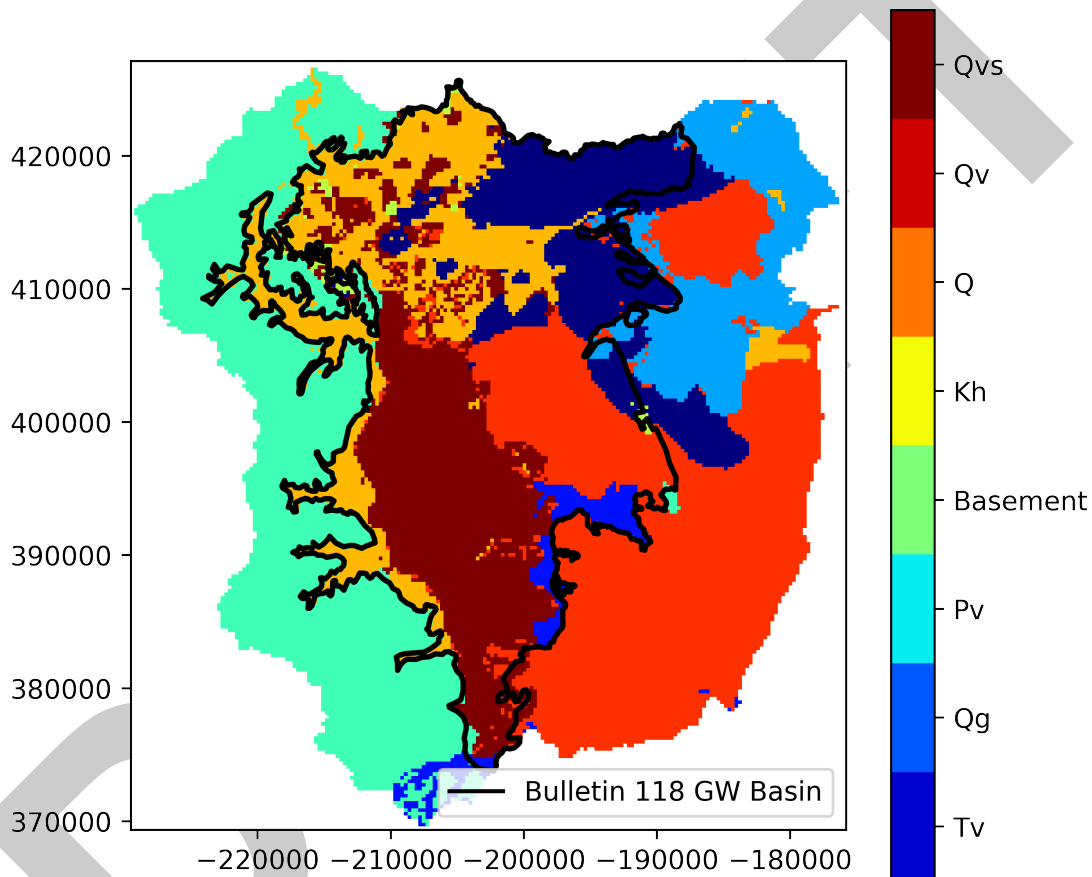


Figure 3: Shasta Valley Geology and model grid discretization

517 Temporal Discretization

518 The SWGM MODFLOW model has monthly stress periods with weekly time steps and runs from
 519 Water Year (WY) 1991-2018. Monthly stress periods are appropriate for the SWGM as the object
 520 of interest is the groundwater budget on the monthly and annual timescale at which groundwater
 521 is typically managed. The SWGM PRMS model uses daily time steps to account for the faster
 522 reaction time typically found in surface water systems.

523 **Agricultural Water Use**

524 Agricultural water use is estimated through the RSRZ, see Appendix 2-I, in combination with land
525 use maps developed by DWR with assistance by local stakeholders (Davids Engineering 2013).

526 **Groundwater Use**

527 Agricultural groundwater use was estimated through the RSRZ. Land irrigated by groundwater, see
528 attached David's Engineering report, were intersected with the RSRZ polygons to create cell-by-cell
529 estimates of groundwater pumping. Groundwater pumping data and pumping well locations were
530 not sufficiently available to allocate groundwater pumping to individual wells, thus groundwater
531 pumping for each node was assigned based on the *Applied Water* calculated by the RSRZ.

532 **Surface Water Use**

533 Surface water diversion are regulated through the Scott and Shasta Watermaster District (SSWD)
534 and the State Water Resource Control Board (SWRCB). Review of historic SSWD reports was
535 compiled by Davids Engineering.

536 The SSWD has seven service areas within the Shasta Watershed; Upper Shasta River, Boles
537 Creek, Beaughan Creek, Carrick Creek, Parks Creek, Lower Shasta River, and Little Shasta River.
538 Annual reports between WY 1991-2017 were considered for review, years with sufficient documen-
539 tation were 1991-1994, 1996-2000, and 2013-2016. Total water rights by service area are shown
540 in Table 3. Table 4 Shows estimated deliveries of water by service region and water year type.
541 For water years with insufficient data, the mean deliveries for that region and water year type were
542 used. The same methodology was used in climate projections when estimating surface water
543 diversions.

Table 3: Total Water Rights by Service Region (shown in cubic feet per second).

| Season | Upper Shasta | Lower Shasta | Little Shasta | Parks Creek | Boles Creek | Beaughan Creek | Carrick Creek | Jackson Creek |
|------------|--------------|--------------|---------------|-------------|-------------|----------------|---------------|---------------|
| Irrigation | 108.66 | 146.64 | 92.32 | 55.66 | 17.68 | 10.30 | 11.72 | 3.05 |
| Winter | 18.55 | 10.85 | 21.93 | 18.33 | 6.99 | 4.47 | 1.39 | 0.38 |

^a Based on Davids Engineering water rights review.

Table 4: Estimates of water deliveries by service region and water year type.

| Month | WY Type | Upper Shasta | Lower Shasta | Little Shasta | Parks Creek | Boles Creek | Beaughan Creek | Carrick Creek | Jackson Creek |
|-----------|---------|--------------|--------------|---------------|-------------|-------------|----------------|---------------|---------------|
| April | Normal | 100% | 98% | 70% | 100% | 100% | 98% | 100% | 100% |
| April | Wet | 100% | 100% | 98% | 100% | 100% | 100% | 100% | 100% |
| April | Dry | 58% | 93% | 27% | 50% | 100% | 100% | 100% | 100% |
| August | Normal | 28% | 90% | 31% | 16% | 100% | 98% | 92% | 100% |
| August | Wet | 59% | 98% | 41% | 15% | 97% | 100% | 100% | 100% |
| August | Dry | 16% | 82% | 26% | 10% | 78% | 100% | 94% | 100% |
| July | Normal | 50% | 93% | 37% | 31% | 100% | 98% | 97% | 100% |
| July | Wet | 91% | 100% | 47% | 34% | 100% | 100% | 100% | 100% |
| July | Dry | 42% | 83% | 29% | 16% | 91% | 100% | 97% | 100% |
| June | Normal | 84% | 97% | 47% | 83% | 100% | 98% | 100% | 100% |
| June | Wet | 100% | 100% | 67% | 85% | 100% | 100% | 100% | 100% |
| June | Dry | 43% | 87% | 41% | 64% | 100% | 100% | 100% | 100% |
| March | Normal | 100% | 98% | 71% | 100% | 100% | 98% | 100% | 100% |
| March | Wet | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% |
| March | Dry | 99% | 97% | 28% | 50% | 100% | 100% | 100% | 100% |
| May | Normal | 100% | 98% | 66% | 98% | 100% | 98% | 100% | 100% |
| May | Wet | 100% | 100% | 91% | 100% | 100% | 100% | 100% | 100% |
| May | Dry | 73% | 87% | 55% | 60% | 100% | 100% | 100% | 100% |
| October | Normal | 6% | 90% | 33% | 3% | 97% | 98% | 88% | 100% |
| October | Wet | 13% | 100% | 39% | 5% | 90% | 100% | 100% | 100% |
| October | Dry | 15% | 82% | 26% | 7% | 74% | 100% | 94% | 100% |
| September | Normal | 7% | 90% | 33% | 5% | 97% | 98% | 90% | 100% |
| September | Wet | 15% | 99% | 39% | 7% | 90% | 100% | 100% | 100% |
| September | Dry | 15% | 82% | 26% | 7% | 74% | 100% | 94% | 100% |

^a Based on Davids Engineering water rights review.

544 **Aquifer Characteristics**

545 **Shasta Watershed Geology**

546 A geologic model was developed to represent the complex geology of the Shasta Watershed. The
 547 geologic model was digitized and included the analysis of hundreds of DWR well logs along with
 548 regional surficial geology maps in Leapfrog⁵. There are 8 hydrogeologic units within the geologic
 549 model which are implemented in the MODFLOW model as listed in Table 4 in Chapter 2 Section
 550 2.1.3. (Appendix 2-A Geologic Modeling Methodology). While there is evidence of faulting oc-
 551 ccurring within the watershed, there was insufficient geologic and hydrologic data to include them
 552 within the groundwater model geology. In addition, fracture flow is known to occur within Qv for-
 553 mation, but due to sparse information of the orientation, size, and connectivity of the fractures the
 554 Qv unit is modeled as equivalent porous media (Appendix 2-A Geologic Modeling Methodology).
 555 The hydraulic properties including horizontal hydraulic conductivity, horizontal anisotropy, vertical
 556 hydraulic conductivity, specific storage, and specific yield, are detailed in Hydraulic Parameters
 557 section. An example cross-section is shown in Figure 4.

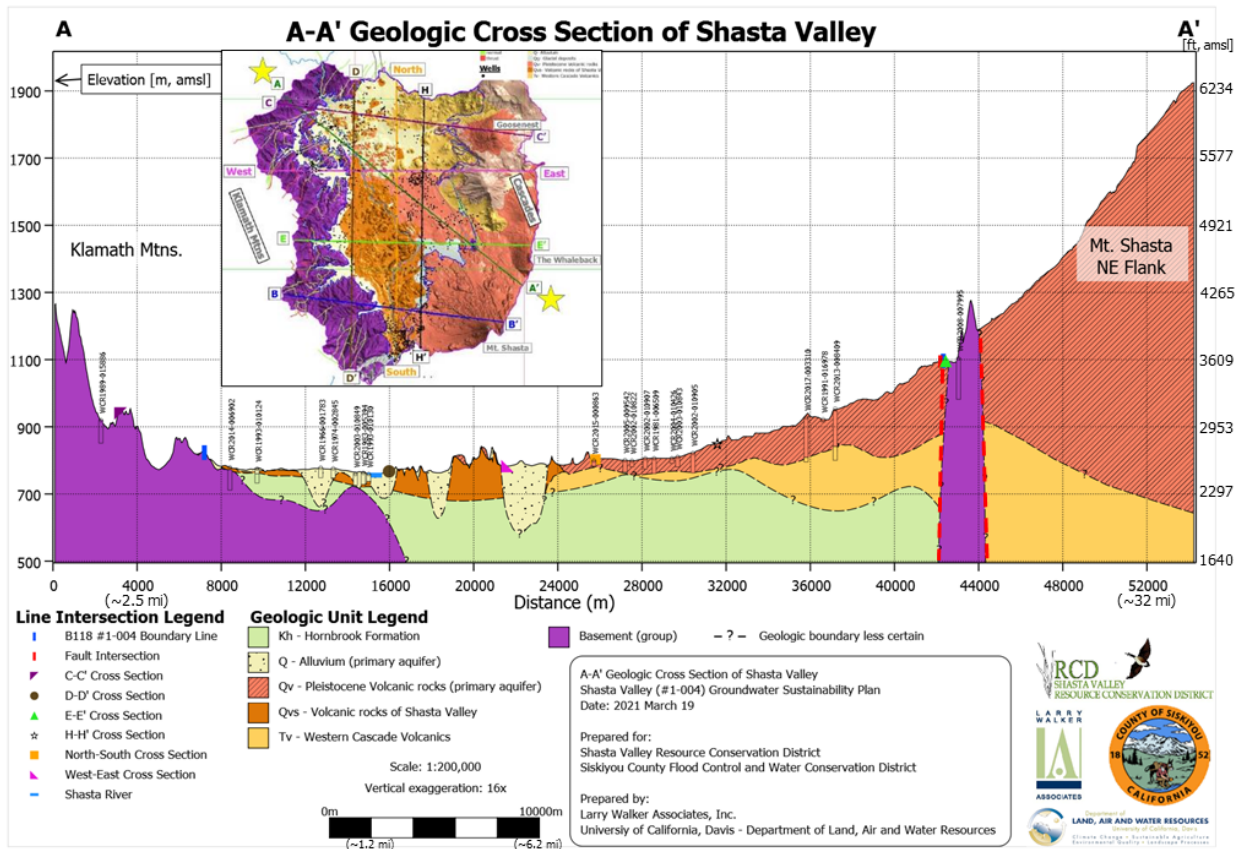


Figure 4: Geologic cross section A-A' from the Shasta Valley Watershed geologic model (inset includes the surface geologic overview map of the Shasta Valley Watershed geologic model).

⁵Sequent, Leapfrog Geo <https://www.sequent.com/products-solutions/leapfrog-geo/>

558 **Hydraulic Properties**

559 **Initial Conditions**

560 The SWGM is initiated with a steady-state model run. Recharge fluxes were estimated using the
561 monthly recharge values before 1997 and averaged. Steady-state flows in the surface water sys-
562 tem were estimated using the average flows in September before 1994. Agricultural pumping was
563 estimated based on the first 9 years, from WY1991-WY1999. Steady-state fluxes were adjusted
564 during model calibration.

565 **Surface Water System**

566 The mainstem of the Shasta River as well as major tributaries are modeled within PRMS and MOD-
567 FLOW. PRMS uses the Muskingum package to route water and MODFLOW uses the Streamflow
568 Routing Package (Niswonger and Prudic 2005). Reach and segment numbering were consistent
569 between PRMS and MODFLOW. The stream network was developed using the same 10-meter
570 resolution DEM from the NED used to establish the topographic setting to derive a representation
571 of the stream system within the Watershed. Stakeholder input was requested to manually correct
572 the DEM-derived stream network due to inaccuracies in elevation as well as the interaction of canal
573 and stream networks.

574 Water conveyance in the Shasta Valley is typically carried out through a complex canal network.
575 Figure 5 shows the entire mapped canal system and the mapped leaky ditches. Leaky ditch desig-
576 nation and locations were provided by the Shasta Valley Resource Conservation District (SVRCD).

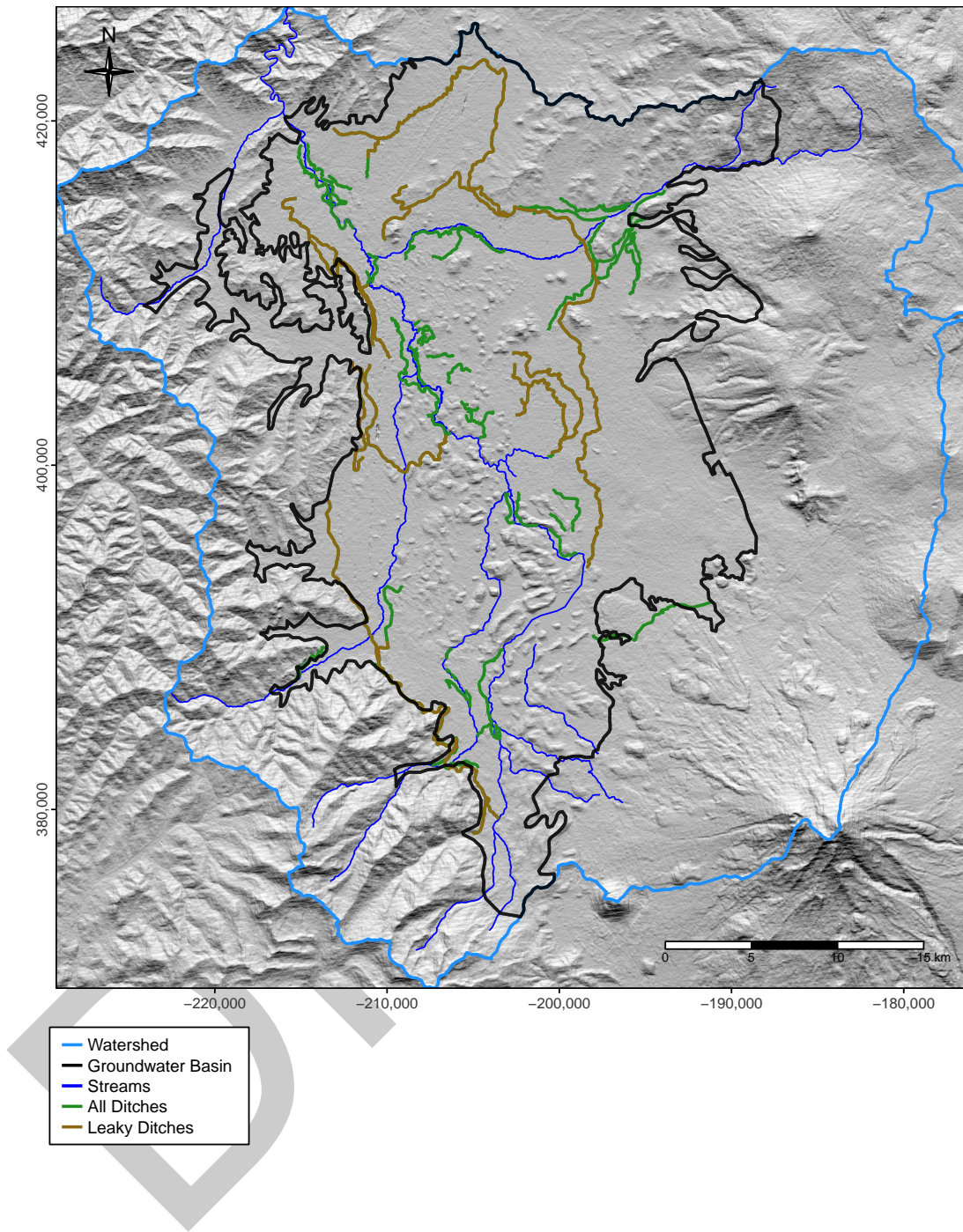


Figure 5: Complete ditch map of Shasta Valley with designation of leaky ditches, as mapped by the SVRCD.

577 Two lakes are modeled in the SWGM, Dwinnell Reservoir and Grass Lake. Dwinnell Reservoir
578 is a managed reservoir with a total capacity of 50,000 acre-feet of water. Inflows to the reservoir
579 are difficult to measure due to the lack of monitoring upstream of the reservoir. The reservoir is
580 fed by the upper Shasta River and various spring fed tributaries. Releases from Dwinnell Reser-
581 voir include instream flow to the Shasta River, prior rights in the Shasta River, and agricultural
582 water demand to the MWCD Canal. Seepage under the dam is also measured and accounted
583 for by MWCD. Releases into the Canal are estimated based on total monthly water deliveries, as
584 submitted to the SWRCB.

585 The complete surface water system as modeled within MODFLOW is shown in Figure 6.

DRAFT

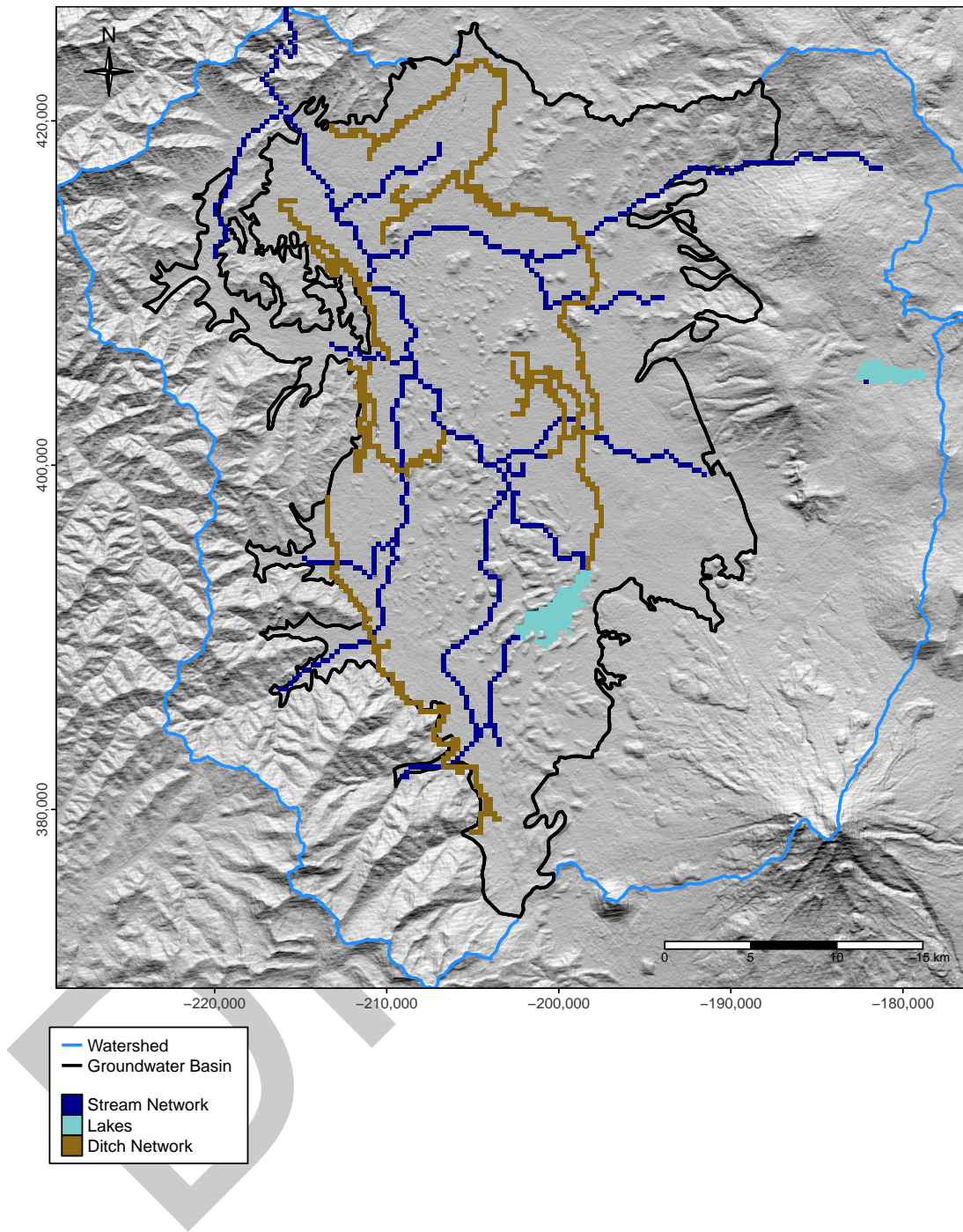


Figure 6: Surface water as modeled within MODFLOW.

586 Model Calibration and Sensitivity

587 The SWGM transient model which ran from WY1991-2018 was calibrated with the groundwater
 588 elevation and streamflow targets described in this section. The sensitivity analysis and calibration
 589 software UCODE2014⁶ was applied to the SWGM. UCODE2014 uses the sum of square weighted
 590 residuals as the objective function for determining the models ability to match observations. Prelim-
 591 inary calibration was conducted on the groundwater flow system but due to data scarcity additional
 592 calibrations will be done for SWGM v1.1. Ongoing recommendations and collaboratoin with the
 593 SWRCB is aiding in constraining the calibration.

594 Observations Used in Model Calibration

595 Groundwater Observations

596 The California Statewide Groundwater Elevation Monitoring (CASGEM) database was filtered and
 597 cleaned for the Shasta Valley area and modeled time period to create a database of groundwater
 598 observations that were corrected with respect to the model top elevations. In addition to the peri-
 599 odic groundwater level measurements, The Nature Conservatory (TNC) has collected groundwater
 600 level data more recently that were included. The groundwater level observations were weighted
 601 using an acceptable standard deviation of 0.1 for observation data from CASGEM and 0.15 for
 602 observation data from TNC. Each well was given a unique name to identify it within the modeling
 603 framework as shown in Table 5. Figures Figure 7, Figure 8, and Figure 9 show the locations of
 604 groundwater elevation wells used in calibration of the SWGM.

Table 5: Overview of Groundwater Elevation Observations

| MODFLOW ID | ROW | COL | Start Date | End Date | No. of Obs |
|-------------------|------------|------------|-------------------|-----------------|-------------------|
| c_10 | 151 | 95 | 1990-10-01 | 2018-03-01 | 54 |
| c_11 | 148 | 121 | 1990-10-01 | 2008-10-01 | 34 |
| c_12 | 139 | 70 | 1990-10-01 | 2018-03-01 | 55 |
| c_13 | 139 | 90 | 1990-10-01 | 2017-10-01 | 55 |
| c_14 | 120 | 65 | 2013-04-01 | 2018-03-01 | 10 |
| c_15 | 115 | 86 | 2005-10-01 | 2018-03-01 | 26 |
| c_16 | 101 | 113 | 1990-10-01 | 2017-10-01 | 54 |
| c_17 | 95 | 111 | 1990-10-01 | 2018-03-01 | 53 |
| c_18 | 43 | 50 | 1990-10-01 | 1992-10-01 | 5 |
| c_19 | 127 | 118 | 1990-10-01 | 2007-03-01 | 31 |
| c_20 | 124 | 62 | 1990-10-01 | 2018-03-01 | 56 |
| c_21 | 113 | 72 | 1990-10-01 | 2018-03-01 | 51 |
| c_22 | 108 | 68 | 1990-10-01 | 2018-03-01 | 55 |
| c_23 | 108 | 88 | 1990-10-01 | 2011-10-01 | 40 |
| c_24 | 105 | 96 | 1990-10-01 | 1997-10-01 | 14 |
| c_25 | 104 | 122 | 1990-10-01 | 2005-10-01 | 29 |
| c_26 | 91 | 109 | 1990-10-01 | 2018-03-01 | 52 |

⁶https://igwmc.mines.edu/wp-content/uploads/sites/117/2018/11/UCODE_2014_User_Manual-version02.pdf

Table 5: Overview of Groundwater Elevation Observations (*continued*)

| MODFLOW ID | ROW | COL | Start Date | End Date | No. of Obs |
|-------------------|------------|------------|-------------------|-----------------|-------------------|
| c_27 | 89 | 93 | 1990-10-01 | 2018-03-01 | 53 |
| c_28 | 81 | 71 | 1990-10-01 | 2018-03-01 | 56 |
| c_29 | 80 | 103 | 1991-03-01 | 2017-10-01 | 52 |
| c_30 | 74 | 110 | 1990-10-01 | 2018-03-01 | 53 |
| c_31 | 66 | 69 | 1990-10-01 | 2018-03-01 | 56 |
| c_32 | 47 | 50 | 1990-10-01 | 2018-03-01 | 55 |
| c_34 | 47 | 96 | 1990-10-01 | 2002-03-01 | 22 |
| c_35 | 46 | 69 | 1990-10-01 | 2018-03-01 | 48 |
| c_36 | 45 | 51 | 2000-09-01 | 2008-10-01 | 18 |
| c_37 | 31 | 93 | 1990-10-01 | 2018-03-01 | 53 |
| c_38 | 30 | 85 | 1990-10-01 | 2018-03-01 | 50 |
| c_39 | 28 | 76 | 1990-10-01 | 2018-03-01 | 45 |
| c_40 | 20 | 104 | 1990-10-01 | 2018-03-01 | 53 |
| c_41 | 18 | 89 | 1990-10-01 | 2018-03-01 | 54 |
| c_42 | 24 | 88 | 2013-04-01 | 2018-03-01 | 9 |
| c_43 | 104 | 89 | 2010-04-01 | 2015-04-01 | 12 |
| c_44 | 74 | 53 | 2004-10-01 | 2018-03-01 | 23 |
| c_45 | 53 | 65 | 2013-04-01 | 2018-03-01 | 11 |
| c_46 | 46 | 76 | 2004-09-01 | 2018-03-01 | 28 |
| TNC_01 | 101 | 98 | 2010-01-01 | 2017-10-01 | 54 |
| TNC_02 | 104 | 89 | 2010-09-01 | 2017-10-01 | 86 |
| TNC_03 | 89 | 93 | 2010-03-01 | 2016-03-01 | 73 |
| TNC_04 | 89 | 93 | 2010-01-01 | 2017-12-01 | 95 |
| TNC_05 | 92 | 103 | 2010-03-01 | 2013-03-01 | 37 |
| TNC_06 | 92 | 103 | 2010-01-01 | 2014-02-01 | 50 |
| TNC_07 | 93 | 103 | 2010-01-01 | 2017-09-01 | 93 |
| TNC_08 | 92 | 102 | 2012-04-01 | 2013-03-01 | 12 |
| TNC_09 | 102 | 101 | 2010-04-01 | 2016-03-01 | 72 |
| TNC_10 | 91 | 99 | 2014-02-01 | 2017-09-01 | 44 |

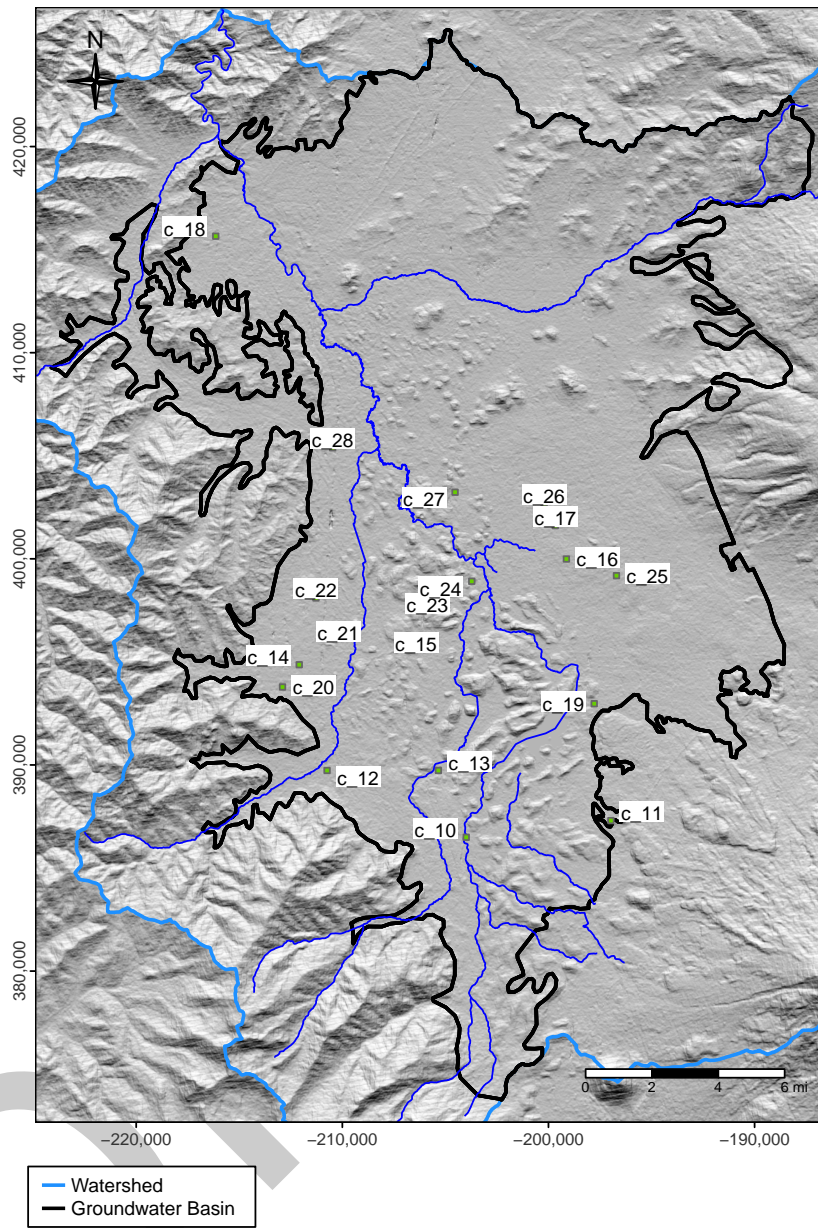


Figure 7: Groundwater Elevation wells used in model calibration, Wells c_10 through c_28.

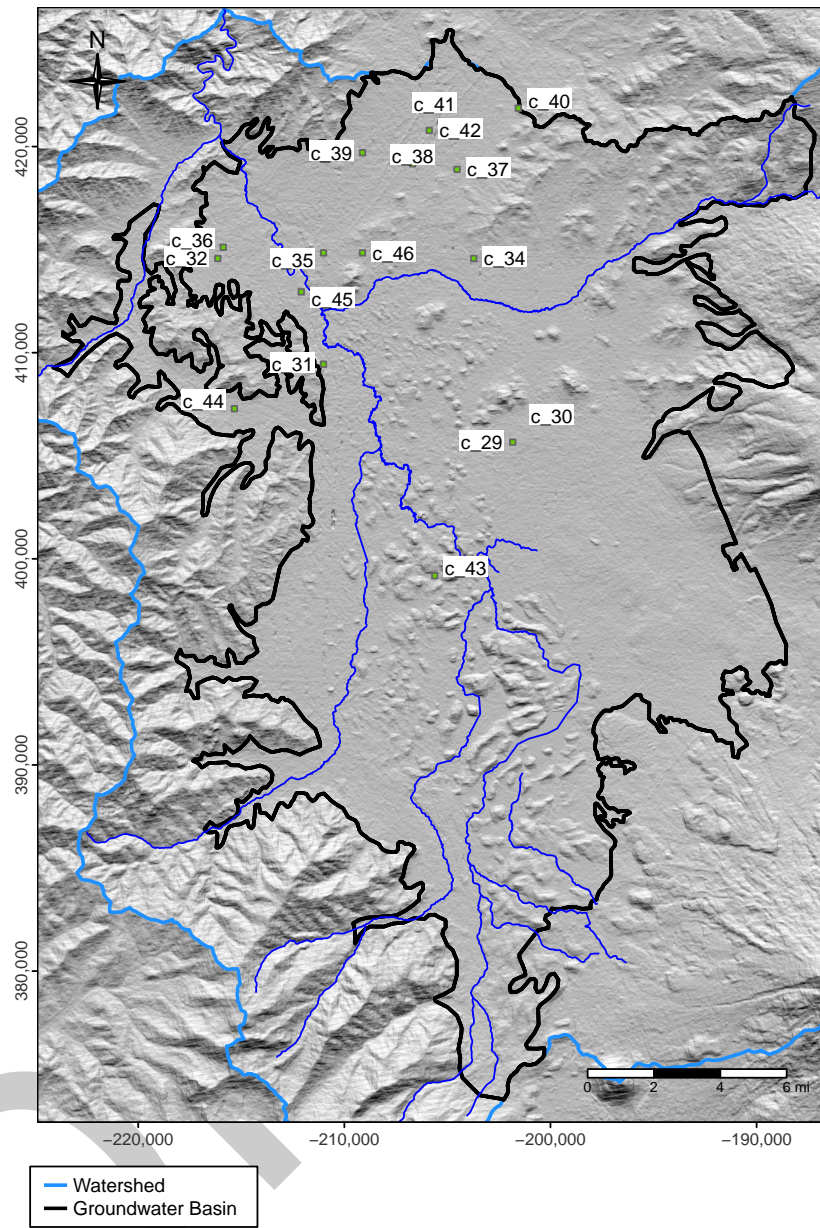


Figure 8: Groundwater Elevation wells used in model calibration, Wells c_29 through c_46.

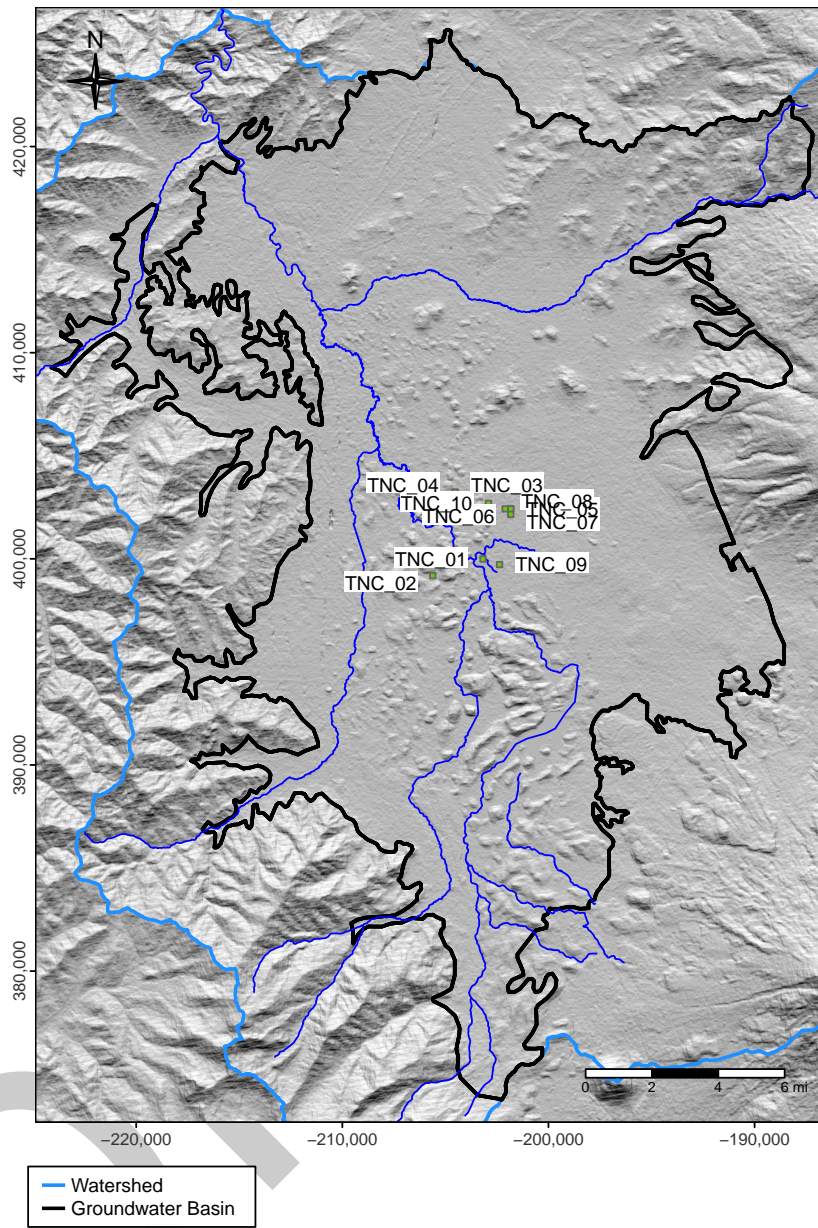


Figure 9: Groundwater Elevation wells used in model calibration, Wells TNC_01 through TNC_10

605 Surface Water Flow Observations

606 Several USGS stream gages exist on the Shasta River and its tributaries which were applied to
 607 both the PRMS and MODFLOW models to calibrate stream and watershed related parameters.
 608 Streamflows measured throughout the upper watershed and Shasta Valley were included as flow
 609 observations with a coefficient of variation of 10% as a weighting parameter.

610 Additional Observations

611 Precipitation gages were used to manually calibrate rainfall distribution within the PRMS model
 612 framework. Remotely sensed snowfall estimations (Bair et al. 2016) were used to examine total
 613 snow pack and the relative distribution of snow within the Shasta Watershed.

614 Model Parameters

615 Hydraulic Parameters

616 There are 41 hydraulic parameters in the SWGM. Table 6 shows the the name of the parameters
 617 as used within the modeling framework in addition to final values used. These parameters are
 618 used exclusively within MODFLOW and control the storage and movement of water through the
 619 subsystem.

Table 6: Hydraulic properites descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|------------|------------|---|
| an1 | HANI | 1.0000000 | Anisotropy multiplier for Unit 1 |
| an2 | HANI | 1.0000000 | Anisotropy multiplier for Unit 2 |
| an3 | HANI | 1.0000000 | Anisotropy multiplier for Unit 3 |
| an4 | HANI | 1.0000000 | Anisotropy multiplier for Unit 4 |
| an5 | HANI | 1.0000000 | Anisotropy multiplier for Unit 5 |
| an6 | HANI | 1.0000000 | Anisotropy multiplier for Unit 6 |
| an7 | HANI | 1.0000000 | Anisotropy multiplier for Unit 7 |
| an8 | HANI | 1.0000000 | Anisotropy multiplier for Unit 8 |
| DRE_leak | LAK | 5.3900000 | Lakebed leakance (BDLKNC) for Dwinnell Reservoir |
| kx1 | HK | 0.0362000 | Horizontal hydraulic conductivity for Unit 1 |
| kx2 | HK | 1.0920000 | Horizontal hydraulic conductivity for Unit 2 |
| kx3 | HK | 0.0111000 | Horizontal hydraulic conductivity for Unit 3 |
| kx4 | HK | 2.4260000 | Horizontal hydraulic conductivity for Unit 4 |
| kx5 | HK | 0.0063900 | Horizontal hydraulic conductivity for Unit 5 |
| kx6 | HK | 12.8910000 | Horizontal hydraulic conductivity for Unit 6 |

Table 6: Hydraulic properties descriptions and values used in the SWGM. (continued)

| Parameter Name | Group Name | Value | Description |
|----------------|------------|------------|--|
| kx7 | HK | 17.1500000 | Horizontal hydraulic conductivity for Unit 7 |
| kx8 | HK | 0.0006650 | Horizontal hydraulic conductivity for Unit 8 |
| kz1 | VK | 16.2800000 | Vertical hydraulic conductivity for Unit 1 |
| kz2 | VK | 44.2900000 | Vertical hydraulic conductivity for Unit 2 |
| kz3 | VK | 5.9460000 | Vertical hydraulic conductivity for Unit 3 |
| kz4 | VK | 0.0294000 | Vertical hydraulic conductivity for Unit 4 |
| kz5 | VK | 0.5002000 | Vertical hydraulic conductivity for Unit 5 |
| kz6 | VK | 16.2900000 | Vertical hydraulic conductivity for Unit 6 |
| kz7 | VK | 66.1400000 | Vertical hydraulic conductivity for Unit 7 |
| kz8 | VK | 0.5590000 | Vertical hydraulic conductivity for Unit 8 |
| ss1 | SS | 0.0003520 | Specific storage for Unit 1 |
| ss2 | SS | 0.0004320 | Specific storage for Unit 2 |
| ss3 | SS | 0.0004140 | Specific storage for Unit 3 |
| ss4 | SS | 0.0001670 | Specific storage for Unit 4 |
| ss5 | SS | 0.0004270 | Specific storage for Unit 5 |
| ss6 | SS | 0.0016300 | Specific storage for Unit 6 |
| ss7 | SS | 0.0000374 | Specific storage for Unit 7 |
| ss8 | SS | 0.0000986 | Specific storage for Unit 8 |
| sy1 | SY | 0.7138000 | Specific yield for Unit 1 |
| sy2 | SY | 0.2500000 | Specific yield for Unit 2 |
| sy3 | SY | 0.2500000 | Specific yield for Unit 3 |
| sy4 | SY | 0.1632000 | Specific yield for Unit 4 |
| sy5 | SY | 0.2510000 | Specific yield for Unit 5 |
| sy6 | SY | 0.0115000 | Specific yield for Unit 6 |
| sy7 | SY | 0.5847000 | Specific yield for Unit 7 |
| sy8 | SY | 0.2731000 | Specific yield for Unit 8 |

620 Soil Parameters

621 There are 16 soil parameters in the SWGM. Table 7 shows the the name of the parameters as used
622 within the modeling framework in addition to final values used. The soil parameters are spatially
623 variable and are based on SSURGO data. Soil modle parameters are generally multipliers to scale
624 the entire basin values. This was done to maintain the spatial distribution of soil properties. These
625 parameters are used within PRMS.

Table 7: Soil properties descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|------------|----------|--|
| care_max | care | 1.000000 | Multiplier for maximum possible area contributing to surface runoff expressed as a portion of the HRU area |
| fastcoef_lin | Soil_Zone | 0.001000 | Linear preferential flow routing coefficient |

Table 7: Soil properties descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|------------|-----------|---|
| fastcoef_sq | Soil_Zone | 0.549791 | Non linear preferential flow routing coefficient |
| pref_flow_den | Soil_Zone | 0.040000 | Fraction of the gravity reservoir in which preferential flow occurs for each HRU |
| sat_threshold | Soil_Zone | 4.560000 | Multiplier for water holding capacity of the gravity and preferential flow reservoirs |
| slowcoef_lin | Soil_Zone | 6.380000 | Multiplier for linear coefficient in equation to route gravity reservoir storage |
| slowcoef_sq | Soil_Zone | 11.020543 | Multiplier for nonlinear coefficient in equation to route gravity reservoir storage downslope |
| smidx_coef | Sroff | 0.100000 | Coefficient in nonlinear contributing area algorithm |
| smidx_exp | Sroff | 0.100000 | Exponent in nonlinear contributing area algorithm |
| soil_moist_max | Soil_Zone | 2.795000 | Multiplier for maximum available water holding capacity of capillary reservoir from land surface to rooting depth |
| soil_rechr_max | Soil_Zone | 1.000000 | Multiplier for maximum storage for soil recharge zone |
| soil2gw_max | Soil_Zone | 0.001000 | Maximum amount of the capillary reservoir excess that is routed directly to the GWR |
| srain_intcp | Intcp | 1.000000 | Multiplier for summer rain interception storage capacity for the major vegetation type |
| ssr2gw_exp | Soil_Zone | 2.400000 | Multiplier for nonlinear coefficient in equation used to route water from the gravity reservoirs to the GWR |
| ssr2gw_rate | Soil_Zone | 1.000000 | Linear coefficient in equation used to route water from the gravity reservoir to the GWR |
| wrain_intcp | Intcp | 3.259831 | Multiplier for winter rain interception storage capacity for the major vegetation type |

626 Climate Parameters

627 There are 103 soil parameters in the SWGM. Table 8 shows the the name of the parameters as
628 used within the modeling framework in addition to final values used. These parameters are used
629 within PRMS.

Table 8: Climate properties descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|-------------|-------------|--|
| adj_rain_apr | adjmix_rain | 1.000000 | Multiplier for rain in April |
| adj_rain_aug | adjmix_rain | 1.000000 | Multiplier for rain in August |
| adj_rain_dec | adjmix_rain | 1.200000 | Multiplier for rain in December |
| adj_rain_feb | adjmix_rain | 1.000000 | Multiplier for rain in February |
| adj_rain_jan | adjmix_rain | 1.000000 | Multiplier for rain in January |
| adj_rain_jul | adjmix_rain | 1.000000 | Multiplier for rain in July |
| adj_rain_jun | adjmix_rain | 1.200000 | Multiplier for rain in June |
| adj_rain_mar | adjmix_rain | 1.000000 | Multiplier for rain in March |
| adj_rain_may | adjmix_rain | 1.000000 | Multiplier for rain in May |
| adj_rain_nov | adjmix_rain | 1.000000 | Multiplier for rain in November |
| adj_rain_oct | adjmix_rain | 1.100000 | Multiplier for rain in October |
| adj_rain_sep | adjmix_rain | 1.000000 | Multiplier for rain in September |
| dday_in_apr | dday_intcp | -7.5759444 | Intercept in degree day equation for PRMS solar radiation in April |
| dday_in_aug | dday_intcp | -34.0000000 | Intercept in degree day equation for PRMS solar radiation in August |
| dday_in_dec | dday_intcp | -8.0000000 | Intercept in degree day equation for PRMS solar radiation in December |
| dday_in_feb | dday_intcp | -7.0000000 | Intercept in degree day equation for PRMS solar radiation in February |
| dday_in_jan | dday_intcp | -12.8721115 | Intercept in degree day equation for PRMS solar radiation in January |
| dday_in_jul | dday_intcp | -37.5030524 | Intercept in degree day equation for PRMS solar radiation in July |
| dday_in_jun | dday_intcp | -13.5515332 | Intercept in degree day equation for PRMS solar radiation in June |
| dday_in_mar | dday_intcp | -7.0000000 | Intercept in degree day equation for PRMS solar radiation in March |
| dday_in_may | dday_intcp | -14.6390135 | Intercept in degree day equation for PRMS solar radiation in May |
| dday_in_nov | dday_intcp | -26.4071231 | Intercept in degree day equation for PRMS solar radiation in November |
| dday_in_oct | dday_intcp | -13.0000000 | Intercept in degree day equation for PRMS solar radiation in October |
| dday_in_sep | dday_intcp | -13.0000000 | Intercept in degree day equation for PRMS solar radiation in September |
| dday_sl_apr | dday_slope | 0.1960800 | Slope in degree day equation for PRMS solar radiation in April |
| dday_sl_aug | dday_slope | 0.6500000 | Slope in degree day equation for PRMS solar radiation in August |
| dday_sl_dec | dday_slope | 0.3100000 | Slope in degree day equation for PRMS solar radiation in December |
| dday_sl_feb | dday_slope | 0.1001000 | Slope in degree day equation for PRMS solar radiation in February |
| dday_sl_jan | dday_slope | 0.3100000 | Slope in degree day equation for PRMS solar radiation in January |
| dday_sl_jul | dday_slope | 0.6989744 | Slope in degree day equation for PRMS solar radiation in July |

Table 8: Climate properties descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|-------------|-----------|---|
| dday_sl_jun | dday_slope | 0.5508728 | Slope in degree day equation for PRMS solar radiation in June |
| dday_sl_mar | dday_slope | 0.3900000 | Slope in degree day equation for PRMS solar radiation in March |
| dday_sl_may | dday_slope | 0.9583546 | Slope in degree day equation for PRMS solar radiation in May |
| dday_sl_nov | dday_slope | 0.6350482 | Slope in degree day equation for PRMS solar radiation in November |
| dday_sl_oct | dday_slope | 0.3400000 | Slope in degree day equation for PRMS solar radiation in October |
| dday_sl_sep | dday_slope | 0.4000000 | Slope in degree day equation for PRMS solar radiation in September |
| freeh2o_cap | snow | 0.0521899 | Free water holding capacity of snowpack |
| pet_adj_apr | Pot_ET | 1.1000000 | Potential ET adjustment in April |
| pet_adj_aug | Pot_ET | 0.8271625 | Potential ET adjustment in August |
| pet_adj_dec | Pot_ET | 1.1252488 | Potential ET adjustment in December |
| pet_adj_feb | Pot_ET | 0.9410774 | Potential ET adjustment in February |
| pet_adj_jan | Pot_ET | 1.1000000 | Potential ET adjustment in January |
| pet_adj_jul | Pot_ET | 0.9000000 | Potential ET adjustment in July |
| pet_adj_jun | Pot_ET | 1.1000000 | Potential ET adjustment in June |
| pet_adj_mar | Pot_ET | 1.0932620 | Potential ET adjustment in March |
| pet_adj_may | Pot_ET | 1.3110423 | Potential ET adjustment in May |
| pet_adj_nov | Pot_ET | 0.8000000 | Potential ET adjustment in November |
| pet_adj_oct | Pot_ET | 1.2000000 | Potential ET adjustment in October |
| pet_adj_sep | Pot_ET | 1.2000000 | Potential ET adjustment in September |
| pet_juniper | Pot_ET | 1.3000000 | Potential ET adjustment in areas with juniper cover |
| pet_other | Pot_ET | 1.1000000 | Potential ET adjustment in areas without juniper cover |
| ppt_radj_apr | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in April |
| ppt_radj_aug | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in August |
| ppt_radj_dec | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in December |
| ppt_radj_feb | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in February |
| ppt_radj_jan | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in January |
| ppt_radj_jul | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in July |
| ppt_radj_jun | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in June |
| ppt_radj_mar | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in March |
| ppt_radj_may | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in May |
| ppt_radj_nov | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in November |
| ppt_radj_oct | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in October |
| ppt_radj_sep | ppt_rad_adj | 0.0200000 | PRMS ppt_rad_adj factor in September |
| radj_sppt | Sol_Rad | 0.3444511 | Adjustment factor for computed solar radiation for summer day with greater than ppt_rad_adj inches of precipitation |
| radj_wppt | Sol_Rad | 0.1277979 | Adjustment factor for computed solar radiation for winter day with greater than ppt_rad_adj inches of precipitation |

Table 8: Climate properties descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|------------|------------|---|
| radmax | Sol_Rad | 0.8000000 | Maximum fraction of the potential solar radiation that may reach the ground due to haze, dust, smog, and so forth |
| tmax_in_apr | tmax_index | 57.4738530 | Index temperature used to determine precipitation adjustments to solar radiation in April |
| tmax_in_aug | tmax_index | 84.3901690 | Index temperature used to determine precipitation adjustments to solar radiation in August |
| tmax_in_dec | tmax_index | 42.1902520 | Index temperature used to determine precipitation adjustments to solar radiation in December |
| tmax_in_feb | tmax_index | 47.0413480 | Index temperature used to determine precipitation adjustments to solar radiation in February |
| tmax_in_jan | tmax_index | 47.5186048 | Index temperature used to determine precipitation adjustments to solar radiation in January |
| tmax_in_jul | tmax_index | 85.0927650 | Index temperature used to determine precipitation adjustments to solar radiation in July |
| tmax_in_jun | tmax_index | 75.1458640 | Index temperature used to determine precipitation adjustments to solar radiation in June |
| tmax_in_mar | tmax_index | 52.1053100 | Index temperature used to determine precipitation adjustments to solar radiation in March |
| tmax_in_may | tmax_index | 66.2615090 | Index temperature used to determine precipitation adjustments to solar radiation in May |
| tmax_in_nov | tmax_index | 49.2785800 | Index temperature used to determine precipitation adjustments to solar radiation in November |
| tmax_in_oct | tmax_index | 64.7301510 | Index temperature used to determine precipitation adjustments to solar radiation in October |
| tmax_in_sep | tmax_index | 77.1708690 | Index temperature used to determine precipitation adjustments to solar radiation in September |
| tmax_lap_apr | tmax_lap | 11.2936403 | Change in maximum air temperature per 1,000 feet elevation change (°F) in April |
| tmax_lap_aug | tmax_lap | 7.0000000 | Change in maximum air temperature per 1,000 feet elevation change (°F) in August |
| tmax_lap_dec | tmax_lap | 12.0000000 | Change in maximum air temperature per 1,000 feet elevation change (°F) in December |

Table 8: Climate properties descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|------------|------------|---|
| tmax_lap_feb | tmax_lap | 12.0000000 | Change in maximum air temperature per 1,000 feet elevation change (°F) in February |
| tmax_lap_jan | tmax_lap | 9.4700610 | Change in maximum air temperature per 1,000 feet elevation change (°F) in January |
| tmax_lap_jul | tmax_lap | 7.5693981 | Change in maximum air temperature per 1,000 feet elevation change (°F) in July |
| tmax_lap_jun | tmax_lap | 5.6314665 | Change in maximum air temperature per 1,000 feet elevation change (°F) in June |
| tmax_lap_mar | tmax_lap | 12.7798857 | Change in maximum air temperature per 1,000 feet elevation change (°F) in March |
| tmax_lap_may | tmax_lap | 11.0000000 | Change in maximum air temperature per 1,000 feet elevation change (°F) in May |
| tmax_lap_nov | tmax_lap | 13.1165216 | Change in maximum air temperature per 1,000 feet elevation change (°F) in November |
| tmax_lap_oct | tmax_lap | 9.6706430 | Change in maximum air temperature per 1,000 feet elevation change (°F) in October |
| tmax_lap_sep | tmax_lap | 9.0000000 | Change in maximum air temperature per 1,000 feet elevation change (°F) in September |
| tmax_snow | tmax_snow | 32.0000000 | Maximum temperature snow can form (°F) |
| tmin_lap_apr | tmin_lap | 7.3058421 | Change in minimum air temperature per 1,000 feet elevation change (°F) in April |
| tmin_lap_aug | tmin_lap | 7.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in August |
| tmin_lap_dec | tmin_lap | 11.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in December |
| tmin_lap_feb | tmin_lap | 11.7491194 | Change in minimum air temperature per 1,000 feet elevation change (°F) in February |
| tmin_lap_jan | tmin_lap | 13.2407952 | Change in minimum air temperature per 1,000 feet elevation change (°F) in January |
| tmin_lap_jul | tmin_lap | 7.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in July |
| tmin_lap_jun | tmin_lap | 8.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in June |
| tmin_lap_mar | tmin_lap | 12.9059633 | Change in minimum air temperature per 1,000 feet elevation change (°F) in March |
| tmin_lap_may | tmin_lap | 15.5359526 | Change in minimum air temperature per 1,000 feet elevation change (°F) in May |

Table 8: Climate properites descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|------------|------------|---|
| tmin_lap_nov | tmin_lap | 2.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in November |
| tmin_lap_oct | tmin_lap | 10.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in October |
| tmin_lap_sep | tmin_lap | 9.0000000 | Change in minimum air temperature per 1,000 feet elevation change (°F) in September |

630 Streamflow Parameters

631 There are 4 streamflow parameters in the SWGM. Table 9 shows the the name of the parameters
 632 as used within the modeling framework in addition to final values used. These parameters are
 633 used within the SFR package of MODFLOW.

Table 9: Streamflow properites descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|------------|--------|---|
| sfr_hc | SFR | 1.2620 | Multiplier for streambed hydraulic conductivity |
| sfr_rough | SFR | 0.5721 | Multiplier for Manning's roughness coefficient |
| sfr_thick | SFR | 0.9254 | Multiplier for streambed thickness |
| sfr_width | SFR | 1.0000 | Multiplier for streambed width |

634 Pumping Parameters

635 There are 13 pumping parameters in the SWGM. Table 10 shows the the name of the parameters
 636 as used within the modeling framework in addition to final values used. These are adjustment
 637 factors to pumping volumes for the entire watershed. They are used within the WEL package of
 638 MODFLOW.

Table 10: Pumping properites descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|------------|-------|--|
| WEL_apr | WEL | 1.0 | Multiplier for all pumping in April |
| WEL_aug | WEL | 1.0 | Multiplier for all pumping in August |
| WEL_dec | WEL | 1.0 | Multiplier for all pumping in December |
| WEL_feb | WEL | 1.0 | Multiplier for all pumping in February |
| WEL_jan | WEL | 1.0 | Multiplier for all pumping in January |
| WEL_jul | WEL | 1.0 | Multiplier for all pumping in July |
| WEL_jun | WEL | 1.0 | Multiplier for all pumping in June |
| WEL_mar | WEL | 1.0 | Multiplier for all pumping in March |

Table 10: Pumping properties descriptions and values used in the SWGM. *(continued)*

| Parameter Name | Group Name | Value | Description |
|----------------|------------|-------|--|
| WEL_may | WEL | 1.0 | Multiplier for all pumping in May |
| WEL_nov | WEL | 1.0 | Multiplier for all pumping in November |
| WEL_oct | WEL | 1.0 | Multiplier for all pumping in October |
| WEL_par | WEL | 1.1 | Multiplier for all pumping in all months |
| WEL_sep | WEL | 1.0 | Multiplier for all pumping in September |

639 Recharge Parameters

640 There are 14 recharge parameters in the SWGM. Table 11 shows the the name of the parameters
641 as used within the modeling framework in addition to final values used. These parameters are
642 adjustment factors to recharge after PRMS and the RSRZ are calculated.

Table 11: Recharge properties descriptions and values used in the SWGM.

| Parameter Name | Group Name | Value | Description |
|----------------|------------|----------|---|
| RCH_apr | UZF | 1.0000 | Recharge multiplier for April |
| RCH_aug | UZF | 1.0000 | Recharge multiplier for August |
| RCH_dec | UZF | 1.0000 | Recharge multiplier for December |
| RCH_feb | UZF | 1.0000 | Recharge multiplier for February |
| RCH_jan | UZF | 1.0000 | Recharge multiplier for January |
| RCH_jul | UZF | 1.0000 | Recharge multiplier for July |
| RCH_jun | UZF | 1.0000 | Recharge multiplier for June |
| RCH_mar | UZF | 1.0000 | Recharge multiplier for March |
| RCH_may | UZF | 1.0000 | Recharge multiplier for May |
| RCH_nov | UZF | 1.0000 | Recharge multiplier for November |
| RCH_oct | UZF | 1.0000 | Recharge multiplier for October |
| RCH_sep | UZF | 1.0000 | Recharge multiplier for September |
| VKS | UZF | 100.0000 | Saturated vertical hydraulic conductivity, used for rejected infiltration only |
| strt_rch | UZF | 0.5579 | Starting recharge multiplier for the steady state stress period |

643 Calibration Results

644 The hydrographs below present the observed groundwater hydrographs versus the simulated
645 heads (after calibration). The map below shows the location of each observation well in the model
646 domain using the MODFLOW node as the naming convention for observations. This is a prelim-
647 inary calibration run. Additional work on including additional observations and changing parame-
648 terization is currently underway in collaboration with the SWRCB.

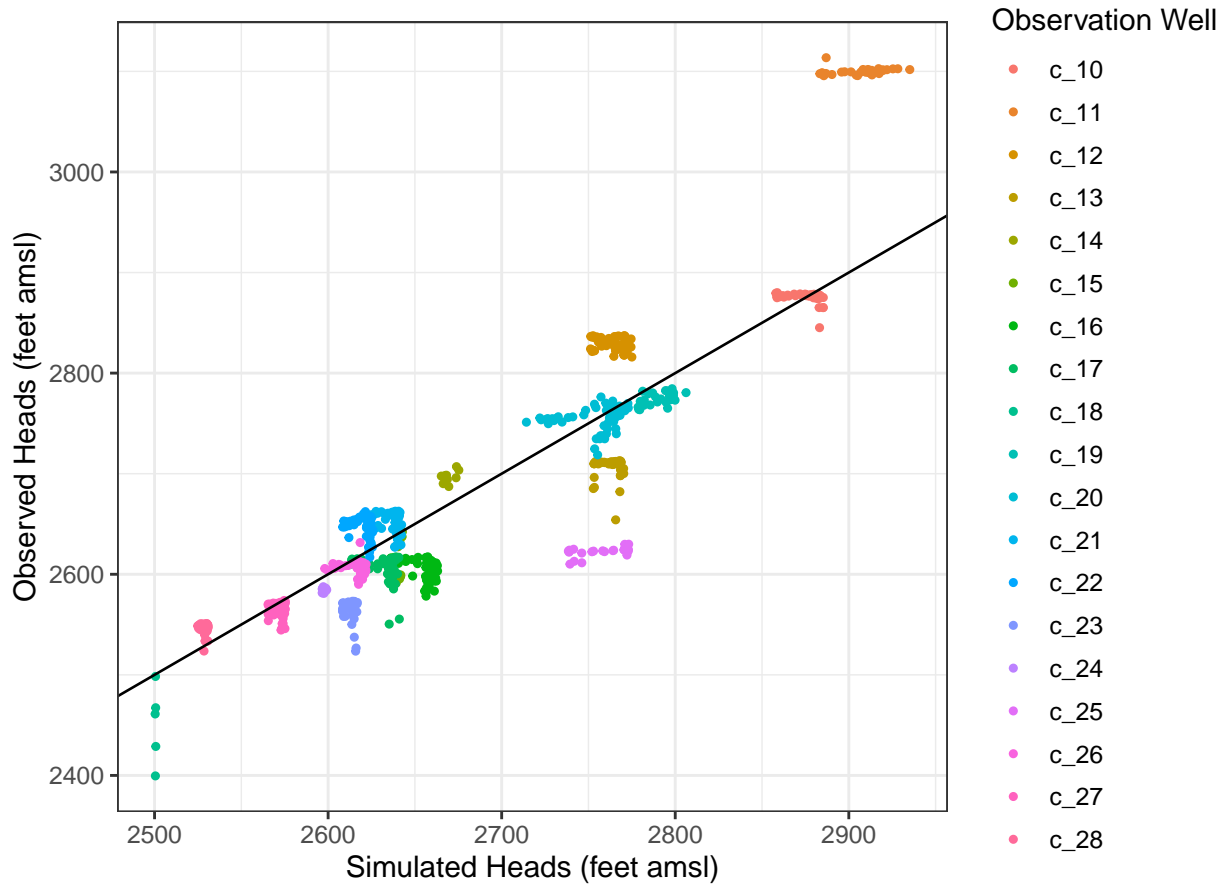


Figure 10: Observed vs. Simulated groundwater elevations in CASGEM Wells (1 of 2).

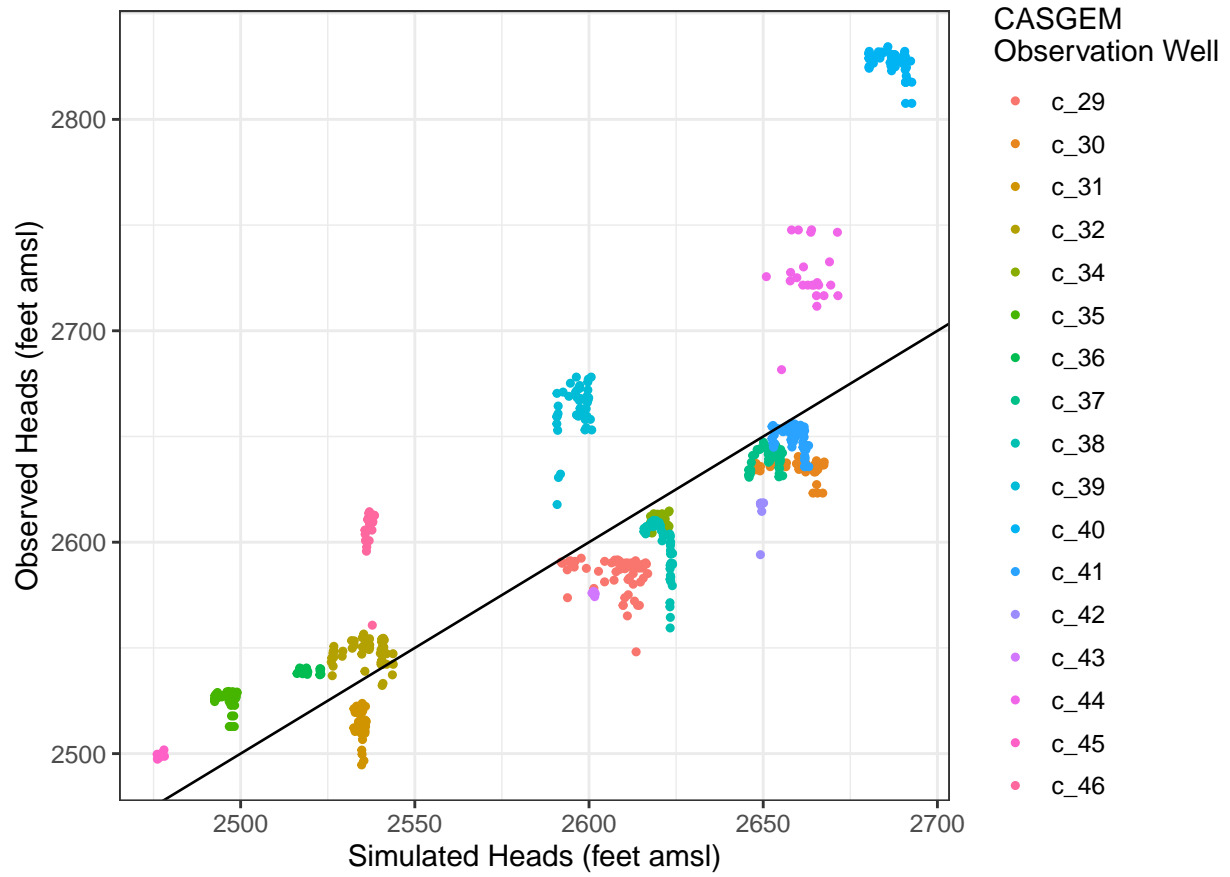


Figure 11: Observed vs. Simulated groundwater elevations in CASGEM Wells (2 of 2).

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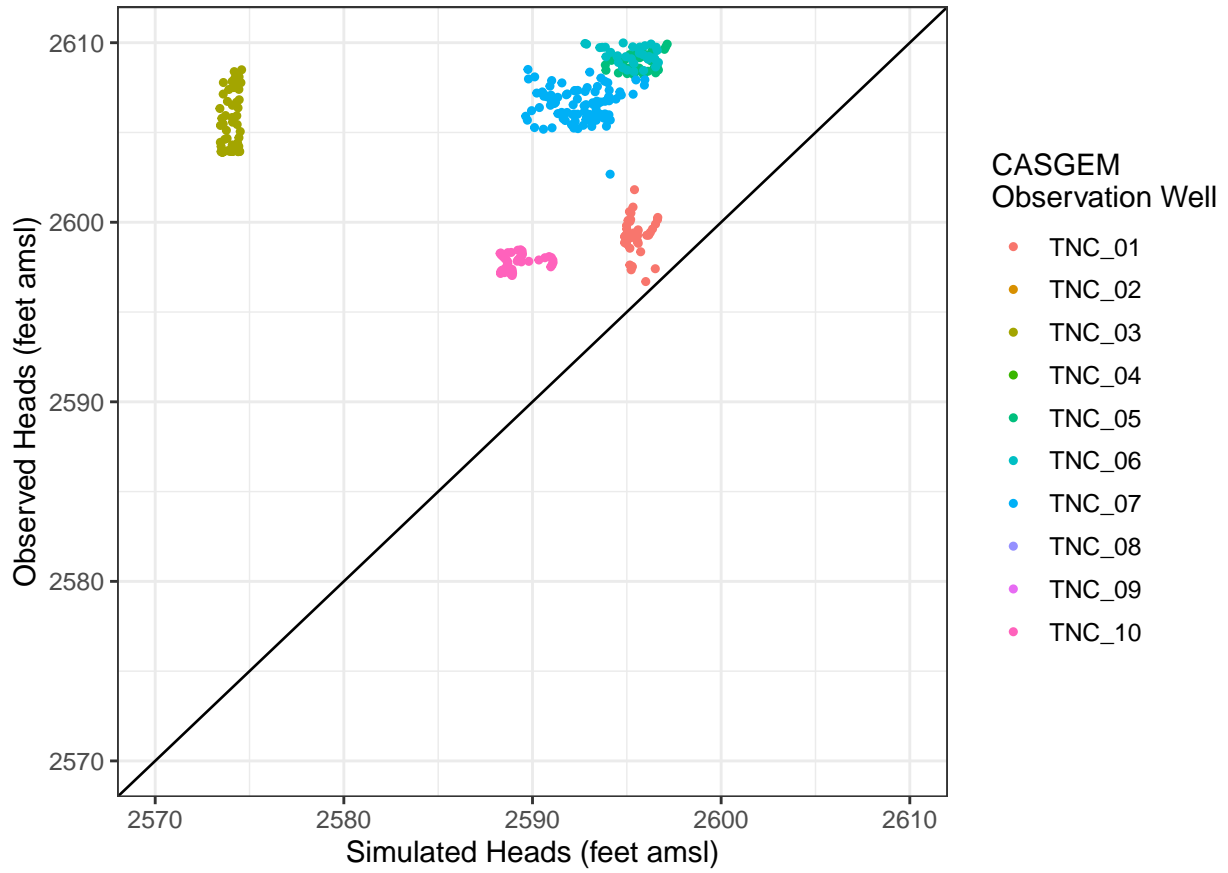


Figure 12: Observed vs. Simulated groundwater elevations in TNC wells near Big Springs.

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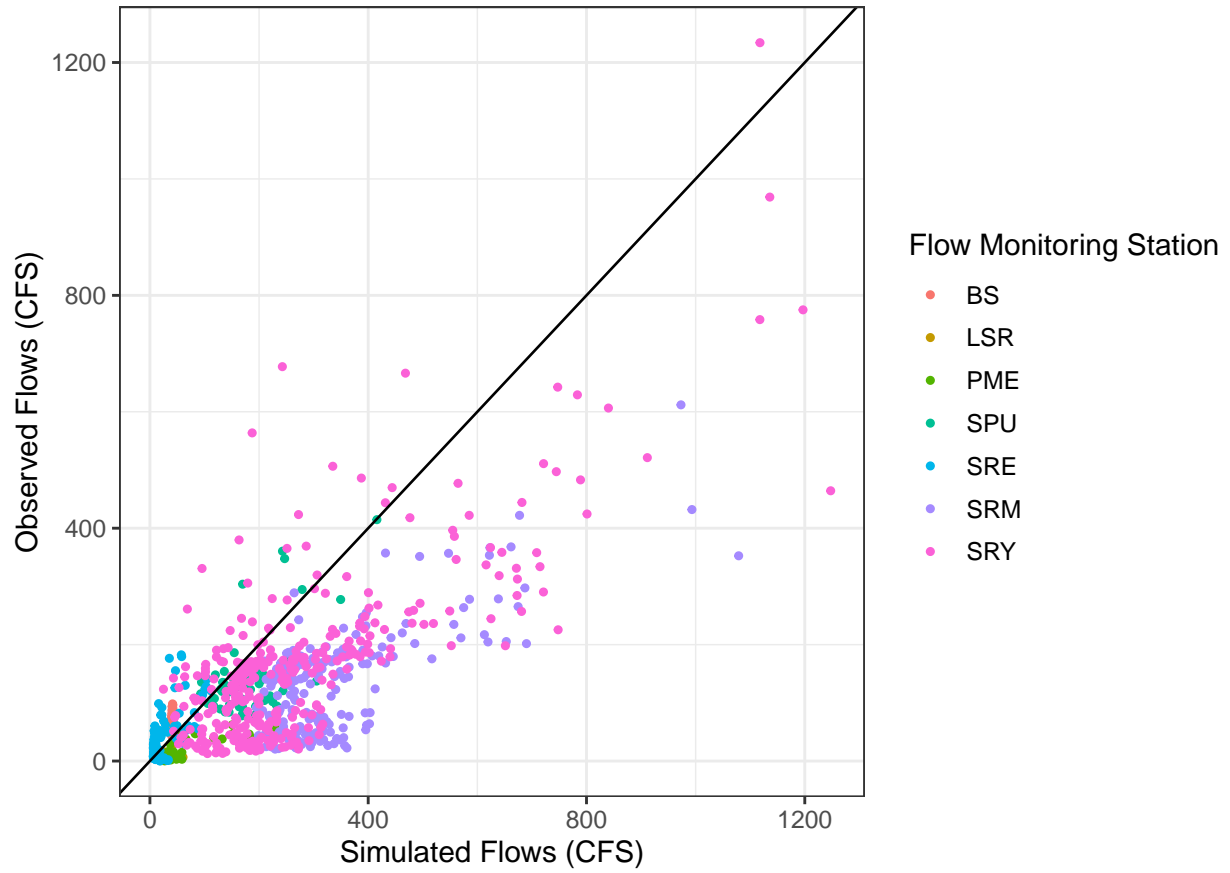


Figure 13: Observed vs. Simulated river flows within Shasta Watershed

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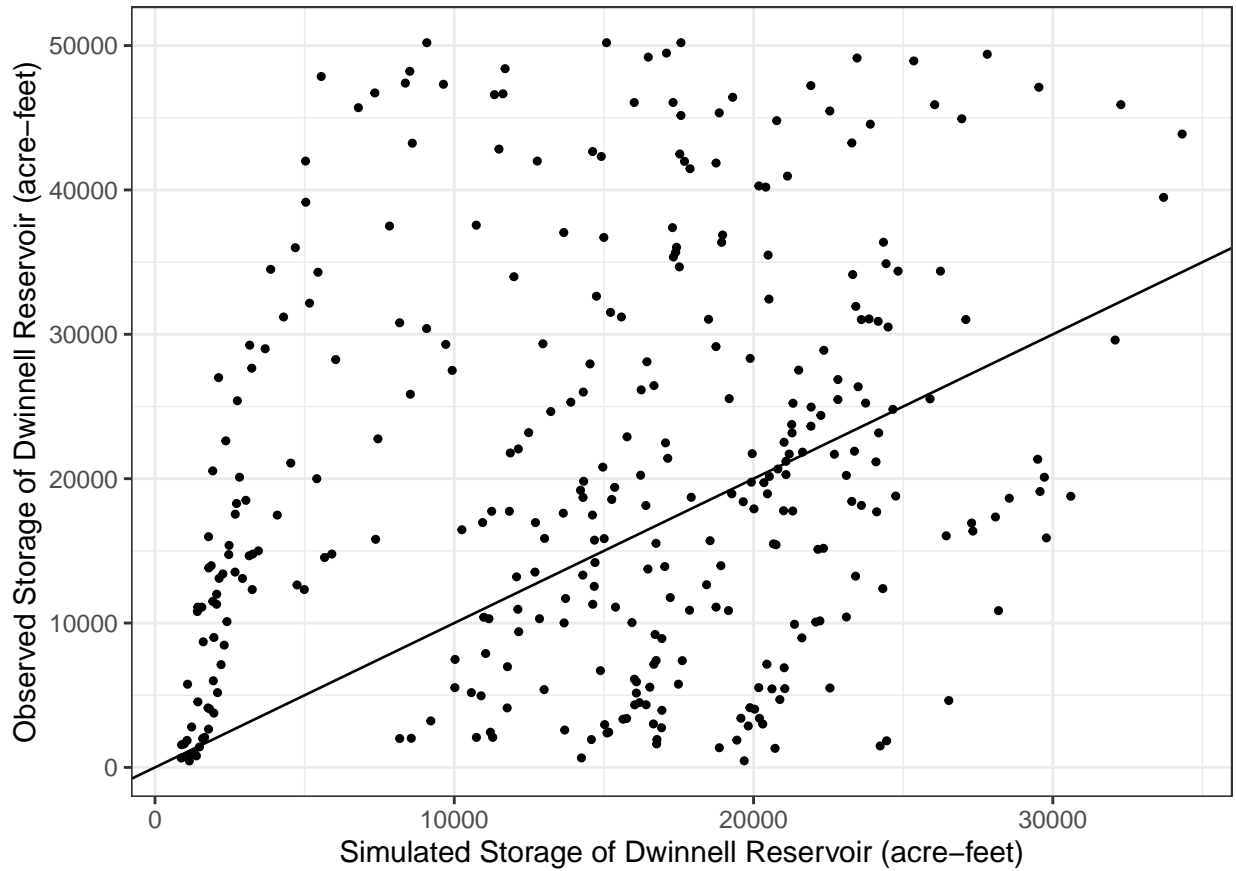


Figure 14: Observed vs. Simulated total storage in Dwinnell Reservoir.

649 **Sensitivity and Uncertainty Analysis**

650 A complete sensitivity and uncertainty analysis will be published in the SWGM v1.1 documentation.

651 **Hydrologic Budget and Flow**

652 **Climate Budget**

653 Climatic water budgets are summarized from PRMS modeled output.

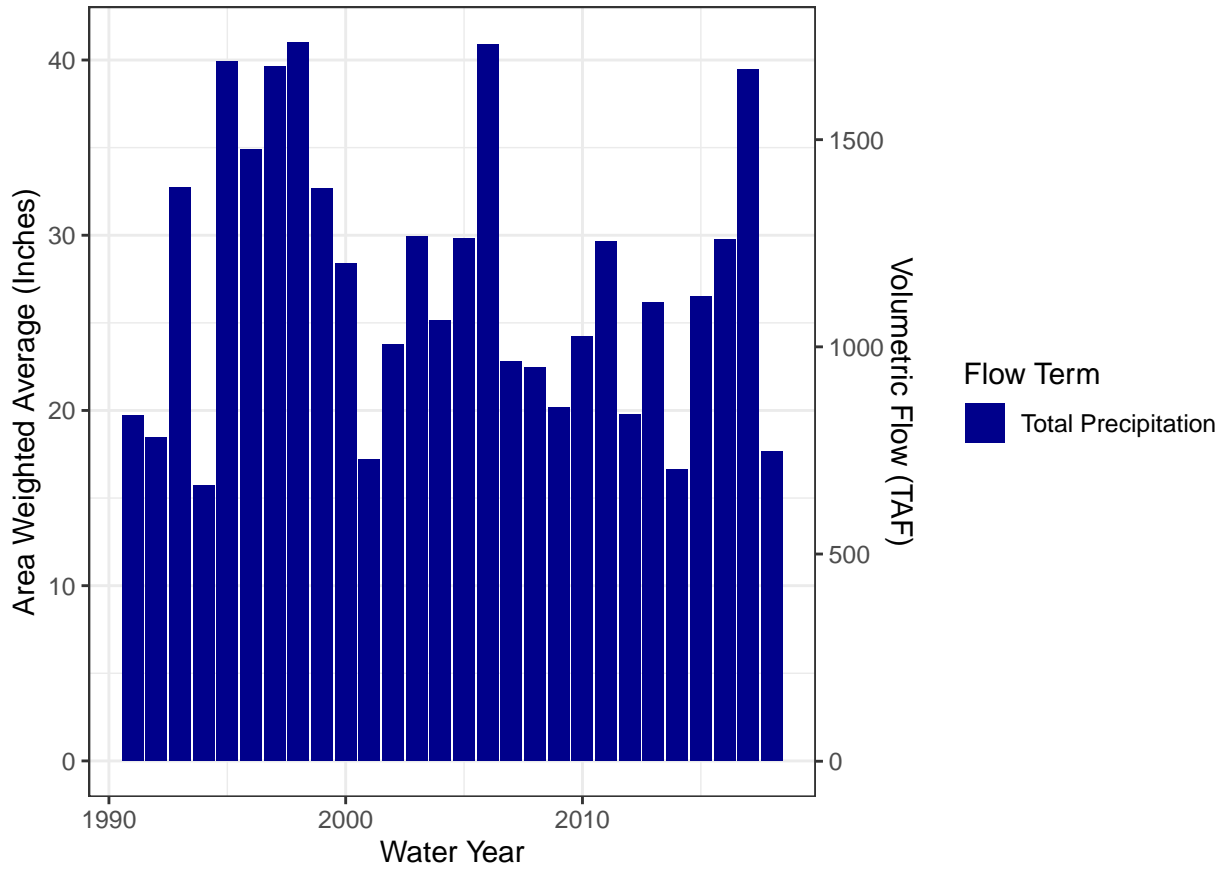


Figure 15: Yearly precipitation within the Shasta Watershed.

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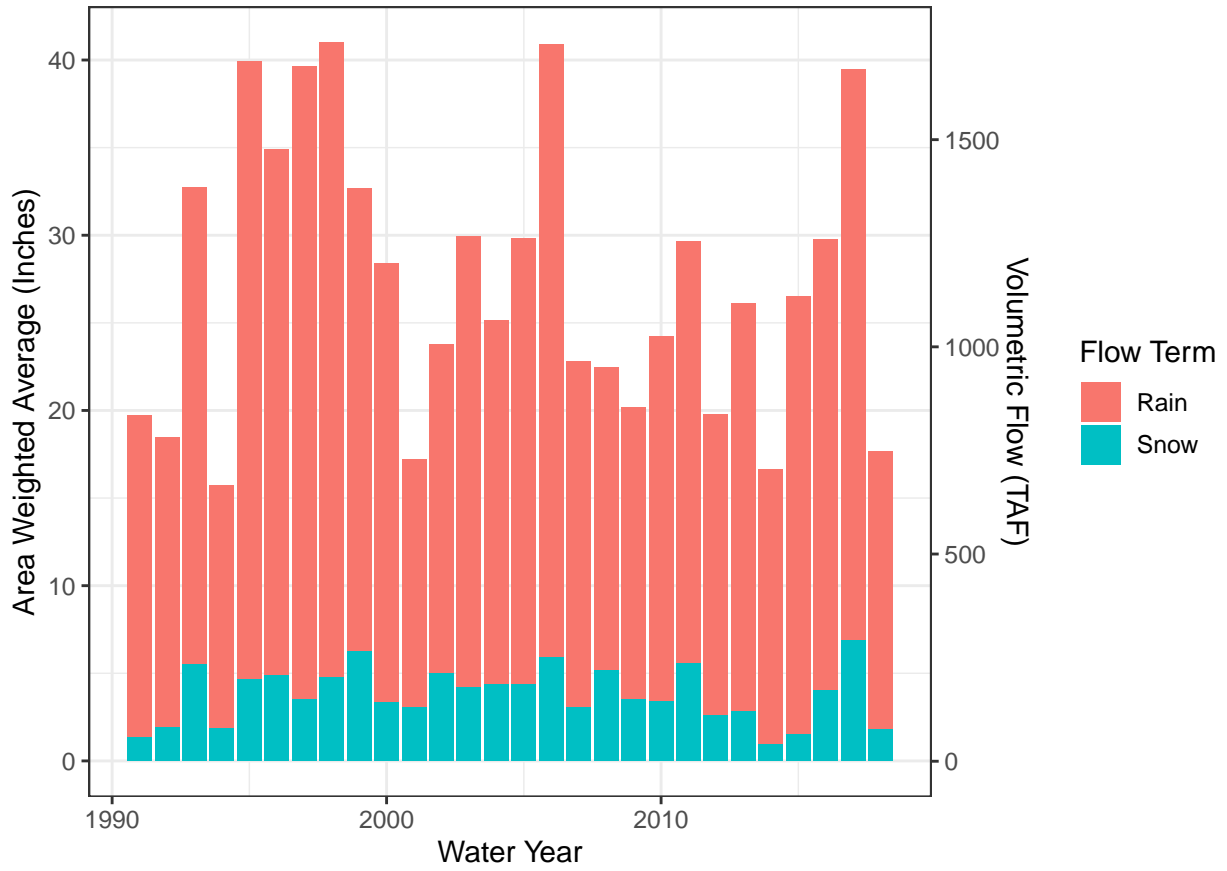


Figure 16: Yearly rain and snowfall within the Shasta Watershed.

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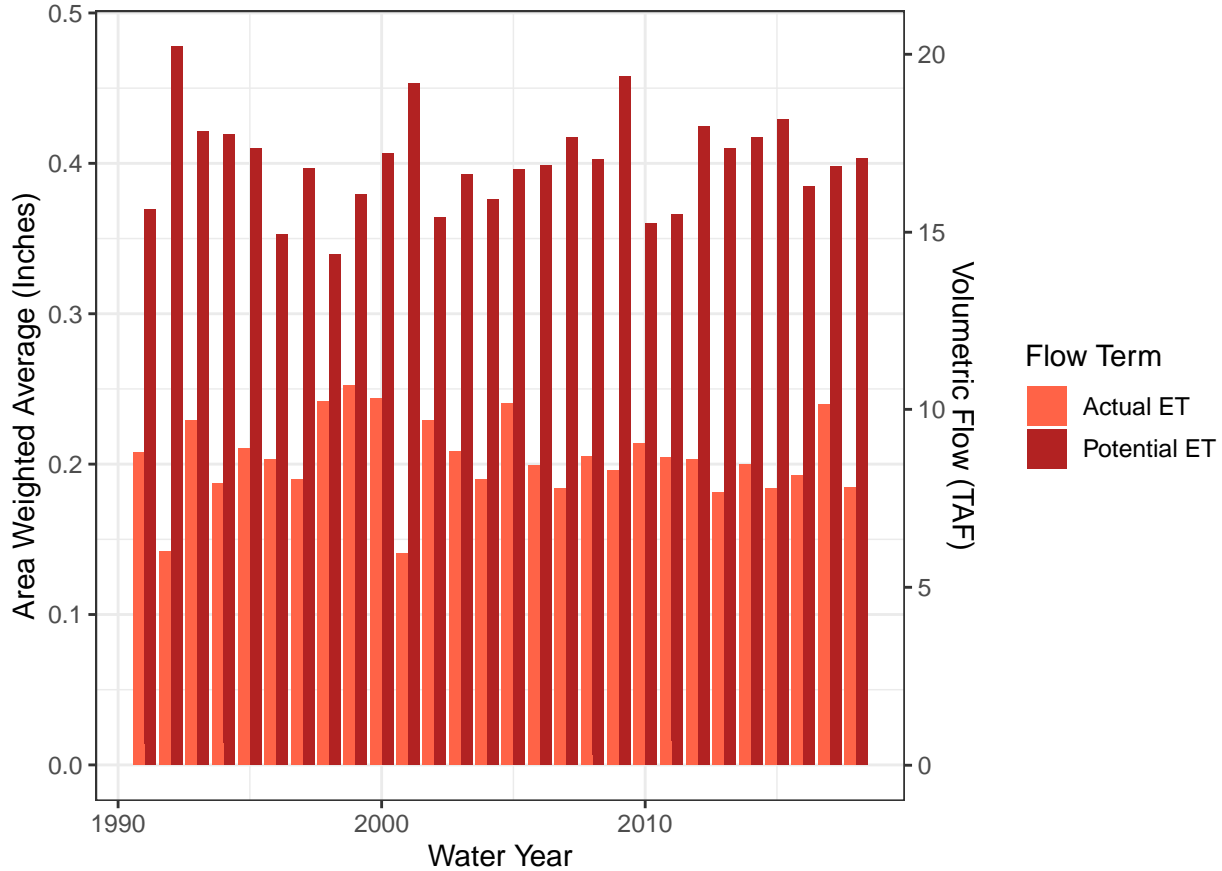


Figure 17: Yearly rain and snowfall within the Shasta Watershed.

654 **Groundwater Budget**

655 Groundwater budgets can be reviewed in Chapter 2 of the Shasta GSP. Updates to the groundwater
 656 budget will be presented in the SWGM v1.1 updated documentation.

657 **Climate Projections**

658 Modeled water balances reflecting a series of climate projections was evaluated with the calibrated
 659 SWGM. Water years were selected from the historic time period (WY1991-WY2018) and repeated
 660 as needed to make a 50-year climate period. The 50-year climate period is recorded as WY2022-
 661 2071. Table 12 shows the sequence of historic climate used to create the projected baseline.

Table 12: Projected climate referenced to historic climate reference years with water year type, as described by DWR, for historic climate.

| Projected Climate | Historic Climate | Water Year Type |
|-------------------|------------------|-----------------|
| 2022 | 1994 | Dry |
| 2023 | 1995 | Wet |

Table 12: Projected climate referenced to historic climate reference years with water year type, as described by DWR, for historic climate. *(continued)*

| Projected Climate | Historic Climate | Water Year Type |
|-------------------|------------------|-----------------|
| 2024 | 1996 | Wet |
| 2025 | 1997 | Wet |
| 2026 | 1998 | Wet |
| 2027 | 1999 | Wet |
| 2028 | 2000 | Above Normal |
| 2029 | 2001 | Critical |
| 2030 | 2002 | Dry |
| 2031 | 2003 | Above Normal |
| 2032 | 2004 | Above Normal |
| 2033 | 2010 | Below Normal |
| 2034 | 2006 | Wet |
| 2035 | 2007 | Below Normal |
| 2036 | 2008 | Dry |
| 2037 | 2009 | Dry |
| 2038 | 2011 | Above Normal |
| 2039 | 1991 | Critical |
| 2040 | 1992 | Critical |
| 2041 | 1993 | Above Normal |
| 2042 | 1994 | Dry |
| 2043 | 1995 | Wet |
| 2044 | 1996 | Wet |
| 2045 | 1997 | Wet |
| 2046 | 1998 | Wet |
| 2047 | 1999 | Wet |
| 2048 | 2000 | Above Normal |
| 2049 | 2001 | Critical |
| 2050 | 2002 | Dry |
| 2051 | 2003 | Above Normal |
| 2052 | 2004 | Above Normal |
| 2053 | 2010 | Below Normal |
| 2054 | 2006 | Wet |
| 2055 | 2007 | Below Normal |
| 2056 | 2008 | Dry |
| 2057 | 2009 | Dry |
| 2058 | 2011 | Above Normal |
| 2059 | 1991 | Critical |
| 2060 | 1992 | Critical |
| 2061 | 1993 | Above Normal |
| 2062 | 1994 | Dry |
| 2063 | 1995 | Wet |
| 2064 | 1996 | Wet |
| 2065 | 1997 | Wet |
| 2066 | 1998 | Wet |
| 2067 | 1999 | Wet |
| 2068 | 2000 | Above Normal |
| 2069 | 2001 | Critical |

Table 12: Projected climate referenced to historic climate reference years with water year type, as described by DWR, for historic climate. (*continued*)

| Projected Climate | Historic Climate | Water Year Type |
|-------------------|------------------|-----------------|
| 2070 | 2002 | Dry |
| 2071 | 2003 | Above Normal |

662 Four climate scenarios were created using the projected baseline climate data, these four sce-
 663 narios are labeled as “Far,” “Near,” “Dry,” and “Wet,” corresponding to DWR future scenarios
 664 “2030”, “2070”, “2070DEW”, and “2070WMW”, respectively. Model differencing was used to ex-
 665 amine trends in different climate scenarios using the baseline projected data as the differencing
 666 base.

667 DWR’s Climate Change Data and Guidance for Use During GSP⁷ development contains a dataset
 668 of “change factors” which each GSA can use to convert local historical weather data into 4 different
 669 climate change scenarios (DWR 2018). Change factors are geographically and temporally explicit.
 670 Geographically, a grid of 1/16-degree resolution cells covers the extent of California; for each of
 671 these cells, one change factors applies to each month, 1911-2011.

672 Under their SGMA climate change guidance, DWR provided a dataset of “change factors” which
 673 each GSA can use to convert local historical weather data into 4 different climate change scenarios
 674 (DWR 2018). Change factors are geographically and temporally explicit. Geographically, a grid
 675 of 1/16-degree resolution cells covers the extent of California; for each of these cells, one change
 676 factors applies to each month, 1911-2011.

677 The 2030 (Near) and 2070 central tendency (Far) scenarios predict similar rainfall conditions to
 678 the Base case, while the 2070 DEW (Dry) and 2070 WMW (Wet) scenarios show less and more
 679 cumulative rain, respectively. Conversely, all scenarios predict higher future ET than the Base
 680 case.

681 Additional information, water budgets, and further discussion on the climate scenario water budgets
 682 will be presented in SWGM v1.1.

683 **Model Limitations and Future Improvements**

684 **Potential Improvements**

685 SWGM v1.0 should be considered a preliminary effort to characterize the Shasta Watershed. Data
 686 from continuous groundwater sensors, increased number of stream gages, and agricultural water
 687 usage will provide updates to the calibrated values of the system. There are a number of updates
 688 that are under consideration for the base model:

- 689 • Updates to glacier melt and snow dynamics on Mount Shasta. Updates to the PRMS code,
 690 v 5.2, include a more robust characterization of glacier dynamics. Increased data collection
 691 on precipitation, solar radiation, air temperature, and other climate variables should also be
 692 included in PRMS updates.

⁷https://groundwaterexchange.org/wp-content/uploads/2020/09/Resource-Guide-Climate-Change-Guidance_v8_ay_19.pdf

- 693 • Geologic updates to include fracture flow within basalt geology.
- 694 • Hydrogeologic updates to refine anisotropy, storage, and model layer thicknesses.
- 695 • Agricultural demands should be internally calculated within the code. Both Ag package within
696 GSFLOW and FMP package with OWHM are possible codes that can be used.
- 697 • Update to stream morphology using LiDAR data from SWRCB.
- 698 • Representation of the canal network using SFR.
- 699 • Update the model simulation period through 2021 to include new continuous groundwater
700 level data collected as part of the GSP.
- 701 • Surface water diversions can be dynamically linked with priorities to the SFR package to meet
702 surface water demand.

703 **Model Archiving**

704 The SWGM will be released to the public after the public comment period and after consulting
705 DWR about best management practices for model release.

706 **References**

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